

# Relativistic Magnetized Jets without Current Sheets

K.N. Gourgouliatos (Purdue)

Collaborators: Ch. Fendt (Heidelberg), J. Braithwaite (Bonn), E. Clausen-Brown (Purdue) & M. Lyutikov (Purdue)

# Outline

- Motivation
- Mathematical Setup
- Static Solution
- Relativistic Solutions
- Simulation
- Stability
- Observational Signature

# Motivation

# Motivation

- We describe the structure of jets containing both plasma and magnetic field

# Motivation

- We describe the structure of jets containing both plasma and magnetic field
- We focus at the region further from the jet engine, where the structure is mainly affected by the boundaries and not very sensitive to the source (i.e. Spruit 2010)

# Motivation

- We describe the structure of jets containing both plasma and magnetic field
- We focus at the region further from the jet engine, where the structure is mainly affected by the boundaries and not very sensitive to the source (i.e. Spruit 2010)
- The external timescales are slow enough, compared to the internal ones, so that the system can reach an equilibrium state

# Motivation

- We describe the structure of jets containing both plasma and magnetic field
- We focus at the region further from the jet engine, where the structure is mainly affected by the boundaries and not very sensitive to the source (i.e. Spruit 2010)
- The external timescales are slow enough, compared to the internal ones, so that the system can reach an equilibrium state
- If the reconnection takes place fast enough we expect that any current sheets will be dissipated

# Physical Question

# Physical Question

- What is the structure of a jet which:

# Physical Question

- What is the structure of a jet which:
  - Contains magnetic field

# Physical Question

- What is the structure of a jet which:
  - Contains magnetic field
  - Contains some hot plasma (pressure)

# Physical Question

- What is the structure of a jet which:
  - Contains magnetic field
  - Contains some hot plasma (pressure)
  - The plasma is moving along the axis

# Physical Question

- What is the structure of a jet which:
  - Contains magnetic field
  - Contains some hot plasma (pressure)
  - The plasma is moving along the axis
  - Is in equilibrium

# Physical Question

- What is the structure of a jet which:
  - Contains magnetic field
  - Contains some hot plasma (pressure)
  - The plasma is moving along the axis
  - Is in equilibrium
  - Has no discontinuities

# Physical Question

• What is the structure of a jet which:

- Contains magnetic field
- Contains some hot plasma (pressure)
- The plasma is moving along the axis
- Is in equilibrium
- Has no discontinuities

• The application:

# Physical Question

• What is the structure of a jet which:

- Contains magnetic field
- Contains some hot plasma (pressure)
- The plasma is moving along the axis
- Is in equilibrium
- Has no discontinuities

• The application:

- Dynamically relaxed structures

# Physical Question

• What is the structure of a jet which:

- Contains magnetic field
- Contains some hot plasma (pressure)
- The plasma is moving along the axis
- Is in equilibrium
- Has no discontinuities

• The application:

- Dynamically relaxed structures
- Endpoints of dissipative evolution

# Physical Question

• What is the structure of a jet which:

- Contains magnetic field
- Contains some hot plasma (pressure)
- The plasma is moving along the axis
- Is in equilibrium
- Has no discontinuities

• The application:

- Dynamically relaxed structures
- Endpoints of dissipative evolution
- Simulation trial solutions - initial conditions

# Mathematical formulation

# Mathematical formulation

- Magnetic flux with poloidal and toroidal components and some plasma are contained within a cylinder

# Mathematical formulation

- Magnetic flux with poloidal and toroidal components and some plasma are contained within a cylinder
- We assume cylindrical symmetry

# Mathematical formulation

- Magnetic flux with poloidal and toroidal components and some plasma are contained within a cylinder
- We assume cylindrical symmetry
- Some hot plasma confines the cylinder

# Mathematical formulation

- Magnetic flux with poloidal and toroidal components and some plasma are contained within a cylinder
- We assume cylindrical symmetry
- Some hot plasma confines the cylinder
- What is the equilibrium solution for this structure?

# Static Solution

# Static Solution

The system consists of two regions:

(I) The magnetized one, which contains magnetic field and hot gas

(II) The external one which contains only hot gas and confines the jet

# Static Solution

The system consists of two regions:

- (I) The magnetized one, which contains magnetic field and hot gas
- (II) The external one which contains only hot gas and confines the jet

The system is everywhere in force equilibrium: the sum of the Lorentz and the pressure gradient is zero (Grad-Shranov Equation)

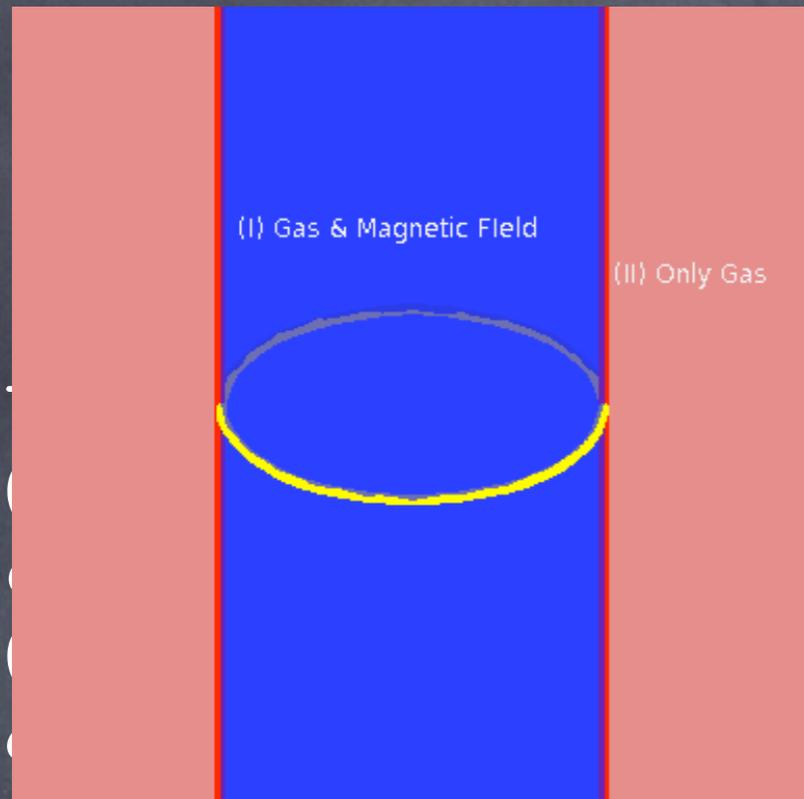
# atic Solution



regions:  
ch  
hot gas  
contains  
the jet

The system is everywhere in force equilibrium: the sum of the Lorentz and the pressure gradient is zero (Grad-Sharanov Equation)

# atic Solution

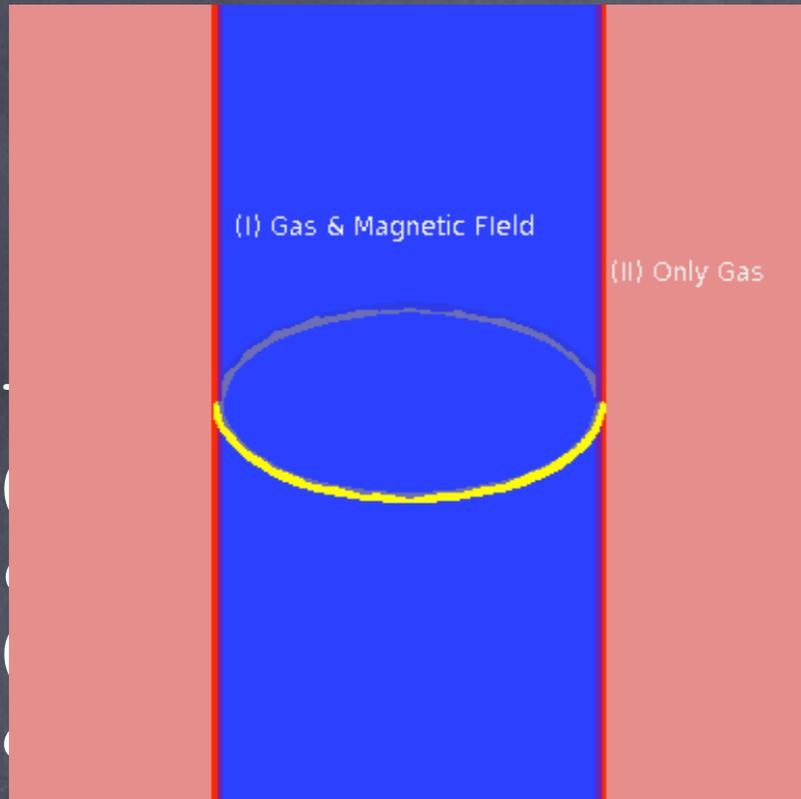


regions:  
ch  
hot gas  
contains  
the jet

The system is everywhere in force equilibrium: the sum of the Lorentz and the pressure gradient is zero (Grad-Shranov Equation)

The boundary condition between regions (I) and (II) is that the magnetic field should drop to zero and there are no current sheets

# atic Solution



regions:  
ch  
hot gas  
contains  
the jet

The system is everywhere in force equilibrium: the sum of the Lorentz and the pressure gradient is zero (Grad-Shranov Equation)

$$\frac{1}{c} \mathbf{j} \times \mathbf{B} = \nabla p$$

The boundary condition between regions (I) and (II) is that the magnetic field should drop to zero and there are no current sheets

# atic Solution



regions:  
ch  
hot gas  
contains  
the jet

The system is everywhere in force equilibrium: the sum of the Lorentz and the pressure gradient is zero (Grad-Shranov Equation)

$$\frac{1}{c} \mathbf{j} \times \mathbf{B} = \nabla p$$

$$(\nabla \times \mathbf{B}) \times \mathbf{B} = 4\pi \nabla p$$

The boundary condition between regions (I) and (II) is that the magnetic field should drop to zero and there are no current sheets

# atic Solution



regions:  
ch  
hot gas  
contains  
the jet

The system is everywhere in force equilibrium: the sum of the Lorentz and the pressure gradient is zero (Grad-Sharanov Equation)

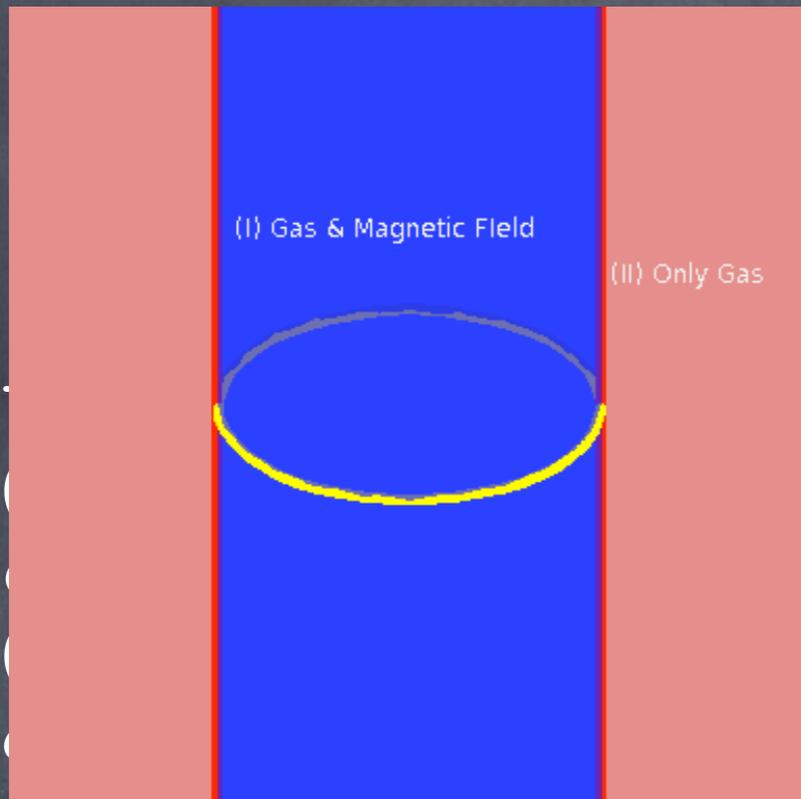
$$\frac{1}{c} \mathbf{j} \times \mathbf{B} = \nabla p$$

$$(\nabla \times \mathbf{B}) \times \mathbf{B} = 4\pi \nabla p$$

The boundary condition between regions (I) and (II) is that the magnetic field should drop to zero and there are no current sheets

We can write a cylindrically symmetric field in two ways: either expressing it in terms of the poloidal flux or the toroidal flux

# atic Solution



regions:  
ch  
hot gas  
contains  
the jet

The system is everywhere in force equilibrium: the sum of the Lorentz and the pressure gradient is zero (Grad-Sharanov Equation)

The boundary condition between regions (I) and (II) is that the magnetic field should drop to zero and there are no current sheets

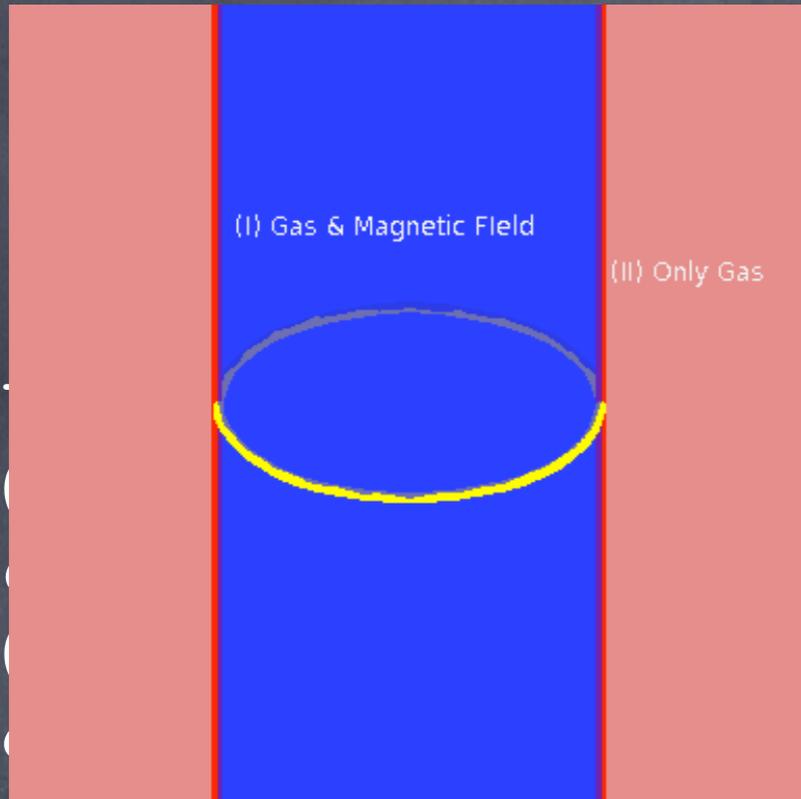
$$\frac{1}{c} \mathbf{j} \times \mathbf{B} = \nabla p$$

$$(\nabla \times \mathbf{B}) \times \mathbf{B} = 4\pi \nabla p$$

$$\mathbf{B} = \nabla P_p(R) \times \nabla \phi + I_p(R) \nabla \phi$$

We can write a cylindrically symmetric field in two ways: either expressing it in terms of the poloidal flux or the toroidal flux

# Static Solution



regions:  
ch  
hot gas  
contains  
the jet

The system is everywhere in force equilibrium: the sum of the Lorentz and the pressure gradient is zero (Grad-Sharanov Equation)

$$\frac{1}{c} \mathbf{j} \times \mathbf{B} = \nabla p$$

$$(\nabla \times \mathbf{B}) \times \mathbf{B} = 4\pi \nabla p$$

The boundary condition between regions (I) and (II) is that the magnetic field should drop to zero and there are no current sheets

$$\mathbf{B} = \nabla P_p(R) \times \nabla \phi + I_p(R) \nabla \phi$$

$$\mathbf{B} = \nabla P_t(R) \times \nabla z + I_t(R) \nabla z$$

We can write a cylindrically symmetric field in two ways: either expressing it in terms of the poloidal flux or the toroidal flux



For the Force-Free case,  
for a linear relation  
between  $P$  and  $I$ , there  
is the Lundquist (1951)  
solution

For the Force-Free case,  
for a linear relation  
between  $P$  and  $I$ , there  
is the Lundquist (1951)  
solution

$$\nabla \times \mathbf{B} = \alpha \mathbf{B}$$

For the Force-Free case,  
for a linear relation  
between  $P$  and  $I$ , there  
is the Lundquist (1951)  
solution

$$\nabla \times \mathbf{B} = \alpha \mathbf{B}$$

$$I_{p,t} = \alpha_{p,t} P_{p,t}$$

For the Force-Free case,  
for a linear relation  
between  $P$  and  $I$ , there  
is the Lundquist (1951)  
solution

$$\nabla \times \mathbf{B} = \alpha \mathbf{B}$$

$$I_{p,t} = \alpha_{p,t} P_{p,t}$$

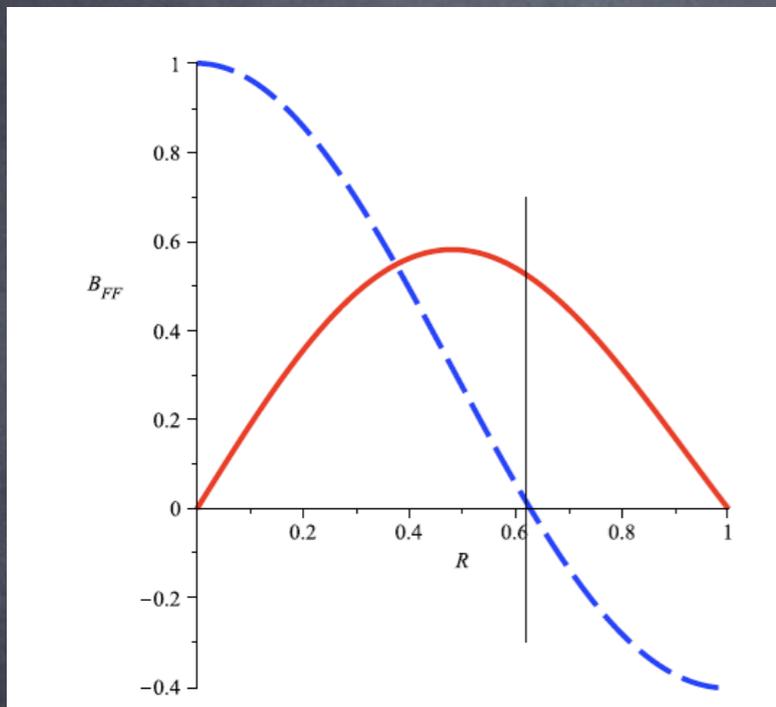
$$\mathbf{B}_{FF} = c_0 \alpha (J_1(\alpha R) \hat{\phi} + J_0(\alpha R) \hat{z})$$

For the Force-Free case,  
for a linear relation  
between  $P$  and  $I$ , there  
is the Lundquist (1951)  
solution

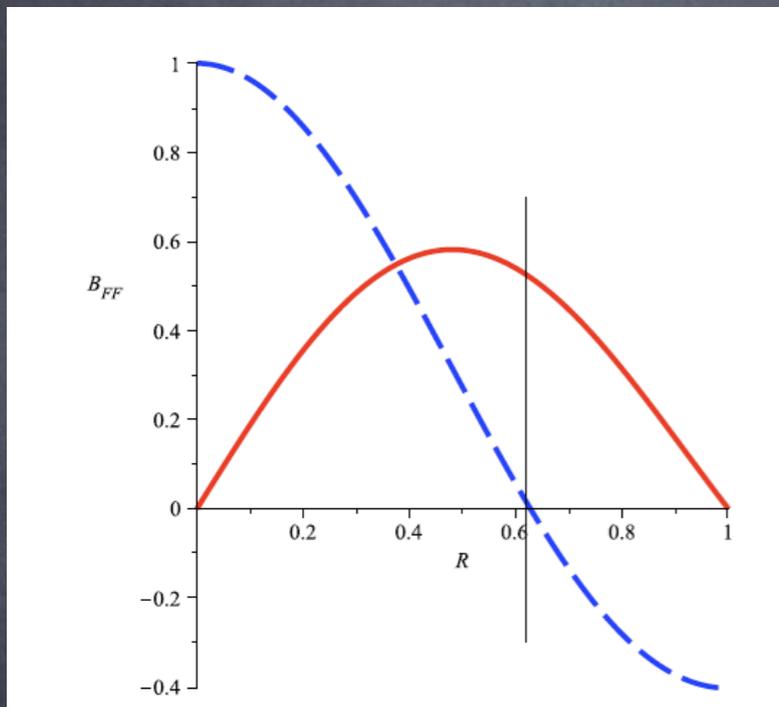
$$\nabla \times \mathbf{B} = \alpha \mathbf{B}$$

$$I_{p,t} = \alpha_{p,t} P_{p,t}$$

$$\mathbf{B}_{FF} = c_0 \alpha (J_1(\alpha R) \hat{\phi} + J_0(\alpha R) \hat{z})$$



For the Force-Free case,  
for a linear relation  
between  $P$  and  $I$ , there  
is the Lundquist (1951)  
solution



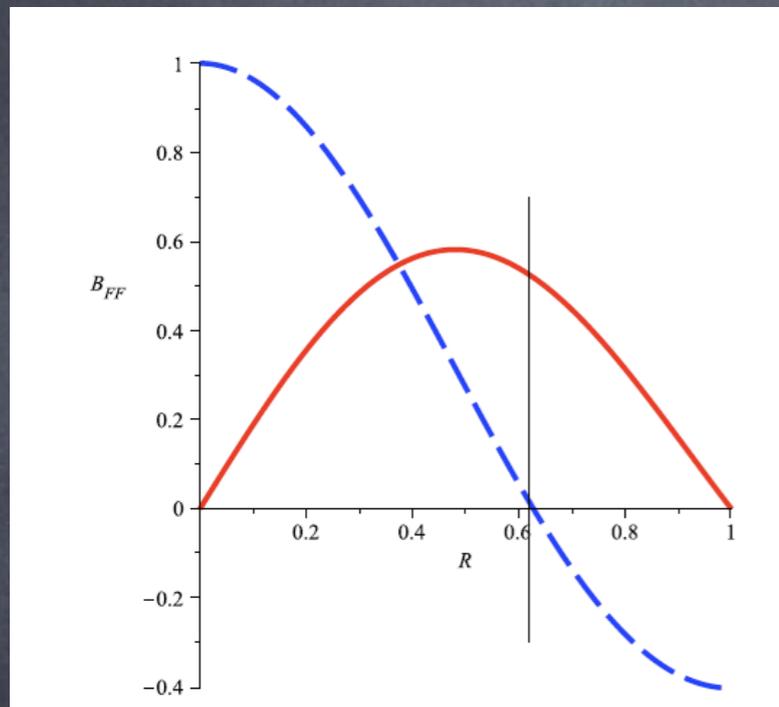
There is no point in the  
Lundquist solution where  
both the toroidal and the  
poloidal field are zero

$$\nabla \times \mathbf{B} = \alpha \mathbf{B}$$

$$I_{p,t} = \alpha_{p,t} P_{p,t}$$

$$\mathbf{B}_{FF} = c_0 \alpha (J_1(\alpha R) \hat{\phi} + J_0(\alpha R) \hat{z})$$

For the Force-Free case, for a linear relation between  $P$  and  $I$ , there is the Lundquist (1951) solution



There is no point in the Lundquist solution where both the toroidal and the poloidal field are zero

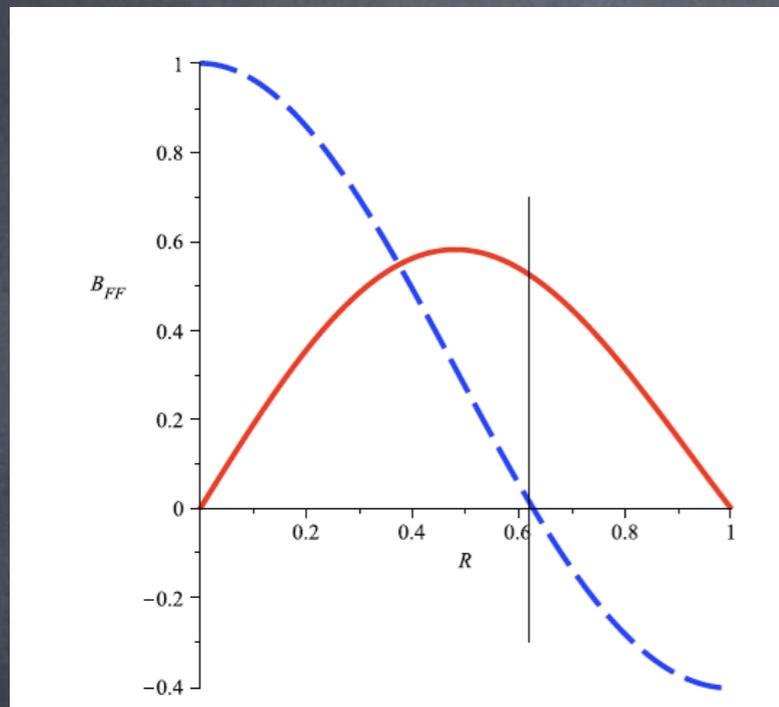
$$\nabla \times \mathbf{B} = \alpha \mathbf{B}$$

$$I_{p,t} = \alpha_{p,t} P_{p,t}$$

$$\mathbf{B}_{FF} = c_0 \alpha (J_1(\alpha R) \hat{\phi} + J_0(\alpha R) \hat{z})$$

In the G-S case there are two classes of solutions, depending on the choice of the pressure: proportional to the poloidal or toroidal flux

For the Force-Free case, for a linear relation between  $P$  and  $I$ , there is the Lundquist (1951) solution



There is no point in the Lundquist solution where both the toroidal and the poloidal field are zero

$$\nabla \times \mathbf{B} = \alpha \mathbf{B}$$

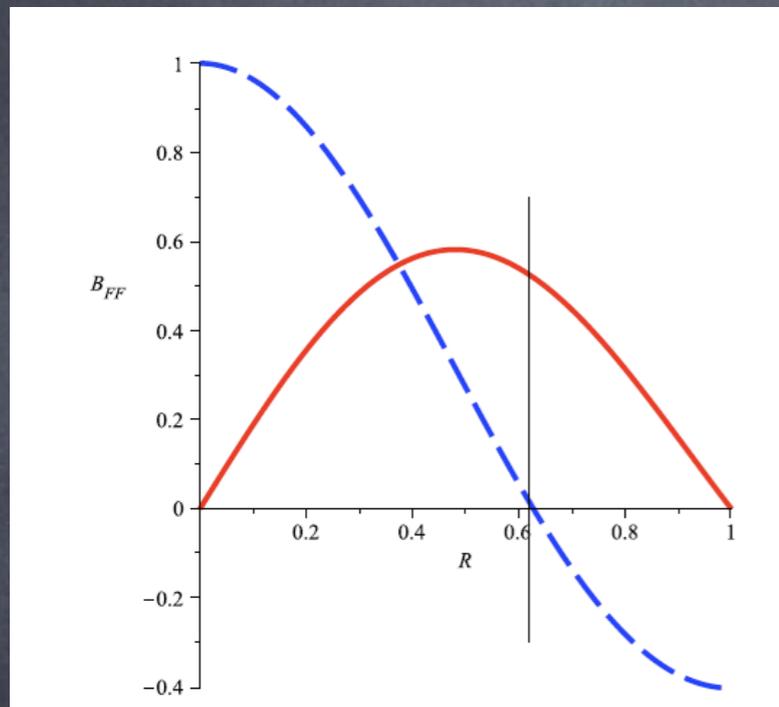
$$I_{p,t} = \alpha_{p,t} P_{p,t}$$

$$\mathbf{B}_{FF} = c_0 \alpha (J_1(\alpha R) \hat{\phi} + J_0(\alpha R) \hat{z})$$

In the G-S case there are two classes of solutions. The choice of the poloidal or toroidal maximum is determined by the equation

$$\frac{R}{2} (B_z^2 + B_\phi^2 + 8\pi p)' + B_\phi^2 = 0$$

For the Force-Free case, for a linear relation between  $P$  and  $I$ , there is the Lundquist (1951) solution



There is no point in the Lundquist solution where both the toroidal and the poloidal field are zero

$$\nabla \times \mathbf{B} = \alpha \mathbf{B}$$

$$I_{p,t} = \alpha_{p,t} P_{p,t}$$

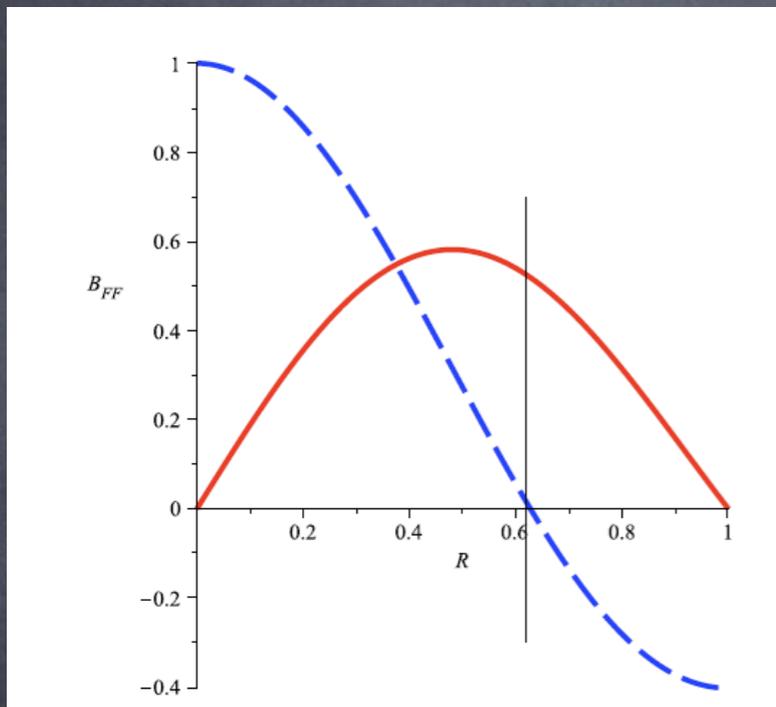
$$\mathbf{B}_{FF} = c_0 \alpha (J_1(\alpha R) \hat{\phi} + J_0(\alpha R) \hat{z})$$

In the G-S case there are two classes of solutions. The choice of the poloidal or toroidal maximum is given by the equation

$$\frac{R}{2} (B_z^2 + B_\phi^2 + 8\pi p)' + B_\phi^2 = 0$$

We can construct two basic families of solutions, where both the toroidal and the poloidal field are zero at the boundary of the cylinder.

For the Force-Free case, for a linear relation between  $P$  and  $I$ , there is the Lundquist (1951) solution



There is no point in the Lundquist solution where both the toroidal and the poloidal field are zero

$$\nabla \times \mathbf{B} = \alpha \mathbf{B}$$

$$I_{p,t} = \alpha_{p,t} P_{p,t}$$

$$\mathbf{B}_{FF} = c_0 \alpha (J_1(\alpha R) \hat{\phi} + J_0(\alpha R) \hat{z})$$

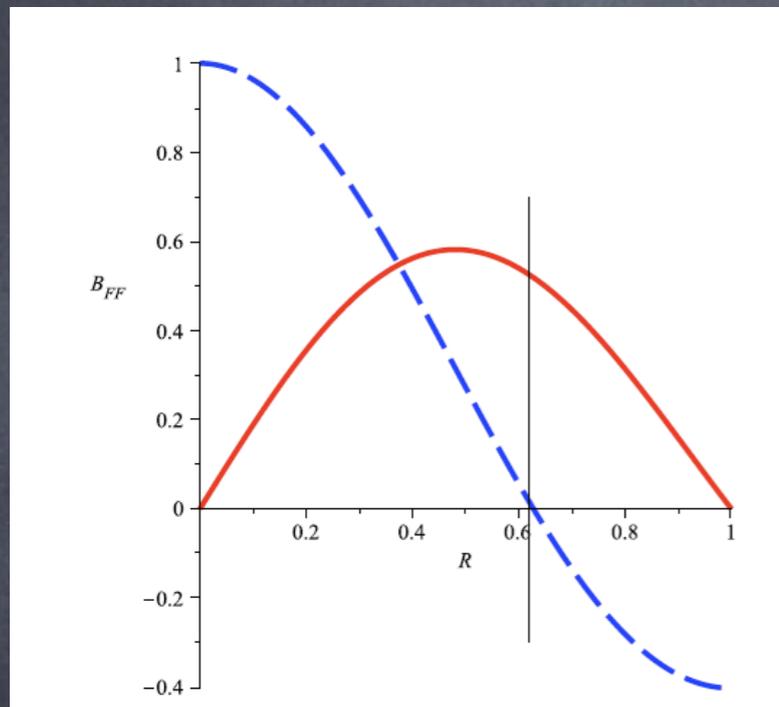
In the G-S case there are two classes of solutions. The choice of the parameter  $\alpha$  determines the poloidal or toroidal flux

$$\frac{R}{2} (B_z^2 + B_\phi^2 + 8\pi p)' + B_\phi^2 = 0$$

$$\mathbf{B}_p = \left( c_p \alpha_p J_1(\alpha_p R) - \frac{F_p R}{\alpha_p} \right) \hat{\phi} +$$

We can construct two basic families of solutions, where both the toroidal and the poloidal field are zero at the boundary of the cylinder.

For the Force-Free case, for a linear relation between  $P$  and  $I$ , there is the Lundquist (1951) solution



There is no point in the Lundquist solution where both the toroidal and the poloidal field are zero

$$\nabla \times \mathbf{B} = \alpha \mathbf{B}$$

$$I_{p,t} = \alpha_{p,t} P_{p,t}$$

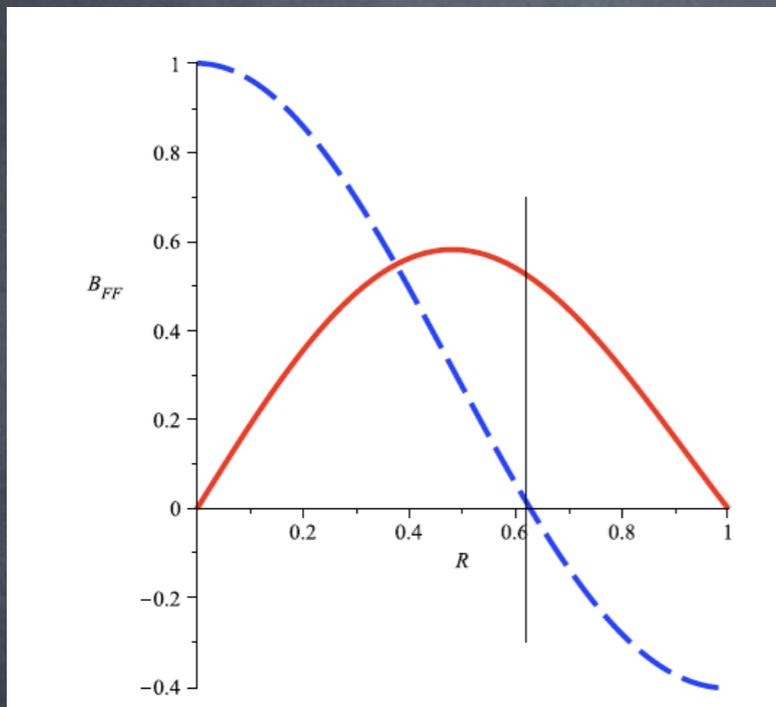
$$\mathbf{B}_{FF} = c_0 \alpha (J_1(\alpha R) \hat{\phi} + J_0(\alpha R) \hat{z})$$

In the G-S case there are two classes of solutions. The choice of the poloidal or toroidal flux is given by the equation  $\frac{R}{2}(B_z^2 + B_\phi^2 + 8\pi p)' + B_\phi^2 = 0$

$$\mathbf{B}_p = \left( c_p \alpha_p J_1(\alpha_p R) - \frac{F_p R}{\alpha_p} \right) \hat{\phi} + \left( c_p \alpha_p J_0(\alpha_p R) - \frac{2F_p}{\alpha_p^2} \right) \hat{z}$$

We can construct two basic families of solutions, where both the toroidal and the poloidal field are zero at the boundary of the cylinder.

For the Force-Free case, for a linear relation between  $P$  and  $I$ , there is the Lundquist (1951) solution



There is no point in the Lundquist solution where both the toroidal and the poloidal field are zero

$$\nabla \times \mathbf{B} = \alpha \mathbf{B}$$

$$I_{p,t} = \alpha_{p,t} P_{p,t}$$

$$\mathbf{B}_{FF} = c_0 \alpha (J_1(\alpha R) \hat{\phi} + J_0(\alpha R) \hat{z})$$

In the G-S case there are two classes of solutions. The choice of the parameter  $\alpha$  is poloidal or toroidal flux

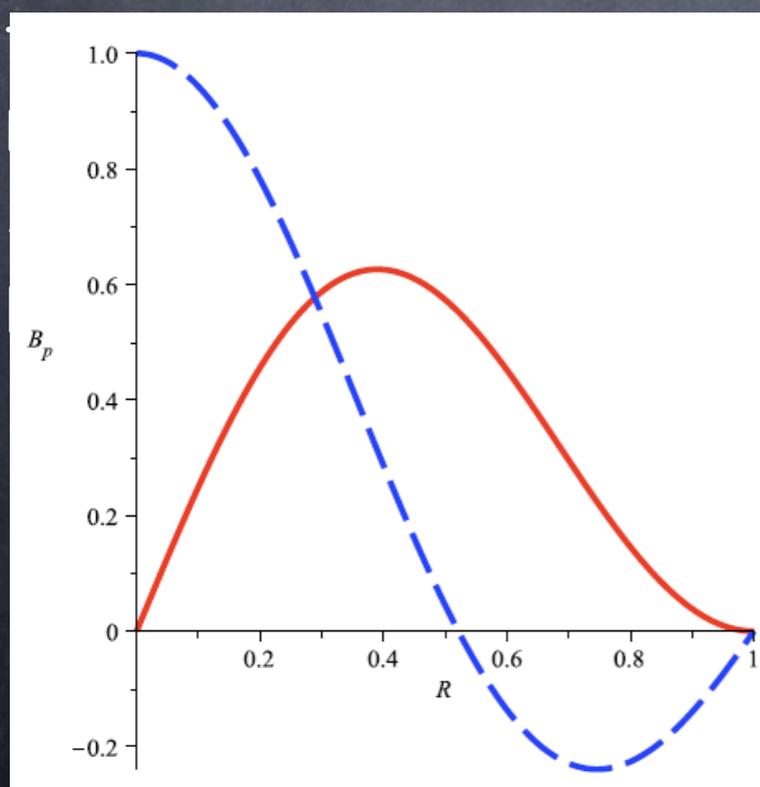
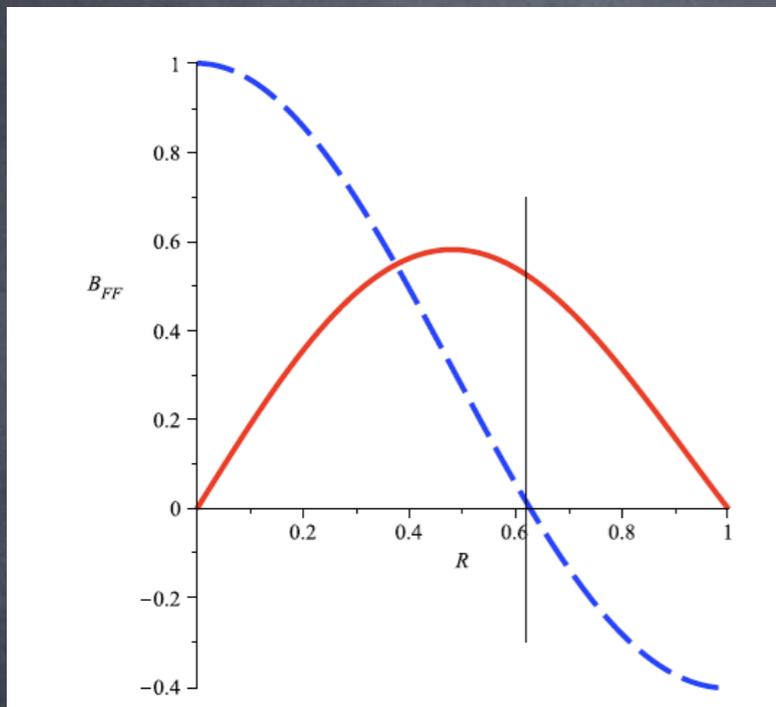
$$\frac{R}{2} (B_z^2 + B_\phi^2 + 8\pi p)' + B_\phi^2 = 0$$

$$\mathbf{B}_p = (c_p \alpha_p J_1(\alpha_p R) - \frac{F_p R}{\alpha_p}) \hat{\phi} + (c_p \alpha_p J_0(\alpha_p R) - \frac{2F_p}{\alpha_p^2}) \hat{z}$$

$$\mathbf{B}_t = c_t \alpha_t J_1(\alpha_t R) \hat{\phi} + (c_t \alpha_t J_0(\alpha_t R) - \frac{F_t}{\alpha_t}) \hat{z}$$

We can construct two basic families of solutions, where both the toroidal and the poloidal field are zero at the boundary of the cylinder.

For the Force-Free case, for a linear relation between  $P$  and  $I$ , there is the Lundquist (1951) solution



$$\nabla \times \mathbf{B} = \alpha \mathbf{B}$$

$$I_{p,t} = \alpha_{p,t} P_{p,t}$$

$$\mathbf{B}_{FF} = c_0 \alpha (J_1(\alpha R) \hat{\phi} + J_0(\alpha R) \hat{z})$$

In the G-S case there are two classes of solutions. The choice of the poloidal or toroidal flux

$$\frac{R}{2} (B_z^2 + B_\phi^2 + 8\pi p)' + B_\phi^2 = 0$$

$$B_p = (c_p \alpha_p J_1(\alpha_p R) - \frac{F_p R}{\alpha_p}) \hat{\phi} + (c_p \alpha_p J_0(\alpha_p R) - \frac{2F_p}{\alpha_p^2}) \hat{z}$$

$$B_t = c_t \alpha_t J_1(\alpha_t R) \hat{\phi} + (c_t \alpha_t J_0(\alpha_t R) - \frac{F_t}{\alpha_t}) \hat{z}$$

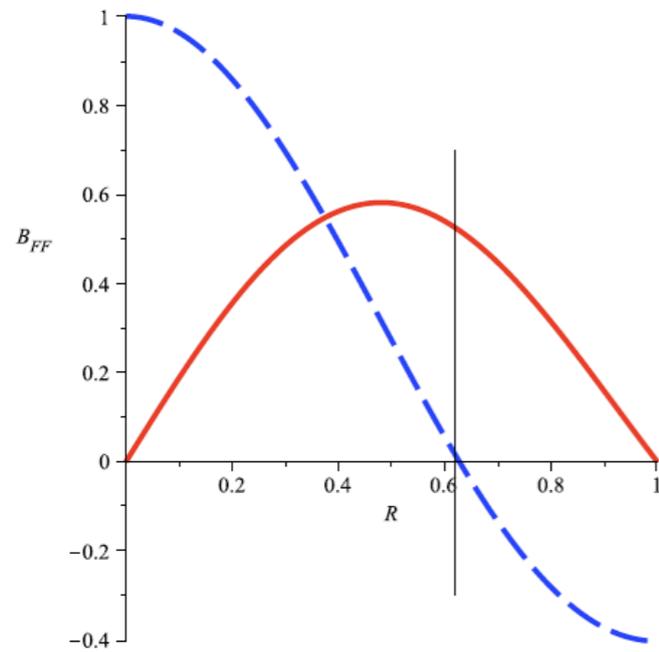
We can construct two basic families of solutions, where both the toroidal and the poloidal field are zero at the boundary of the cylinder.

For the Force-Free case, for a linear relation between  $P$  and  $I$ , there is the Lundquist (1951) solution

$$\nabla \times \mathbf{B} = \alpha \mathbf{B}$$

$$I_{p,t} = \alpha_{p,t} P_{p,t}$$

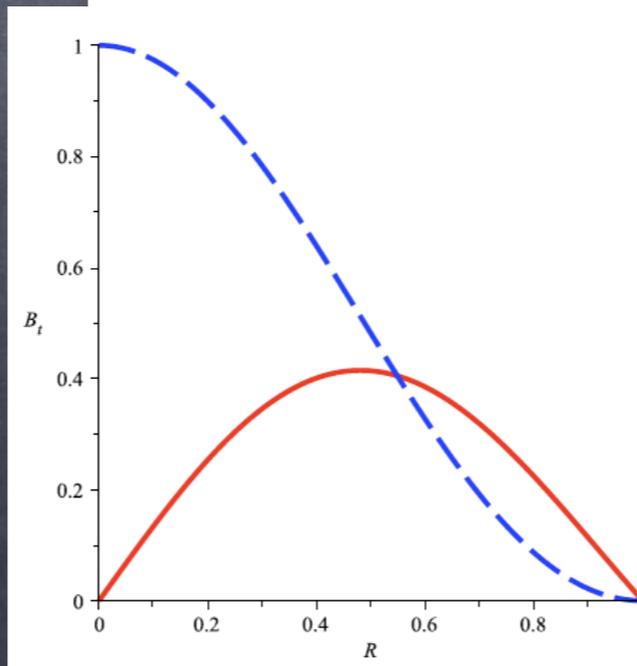
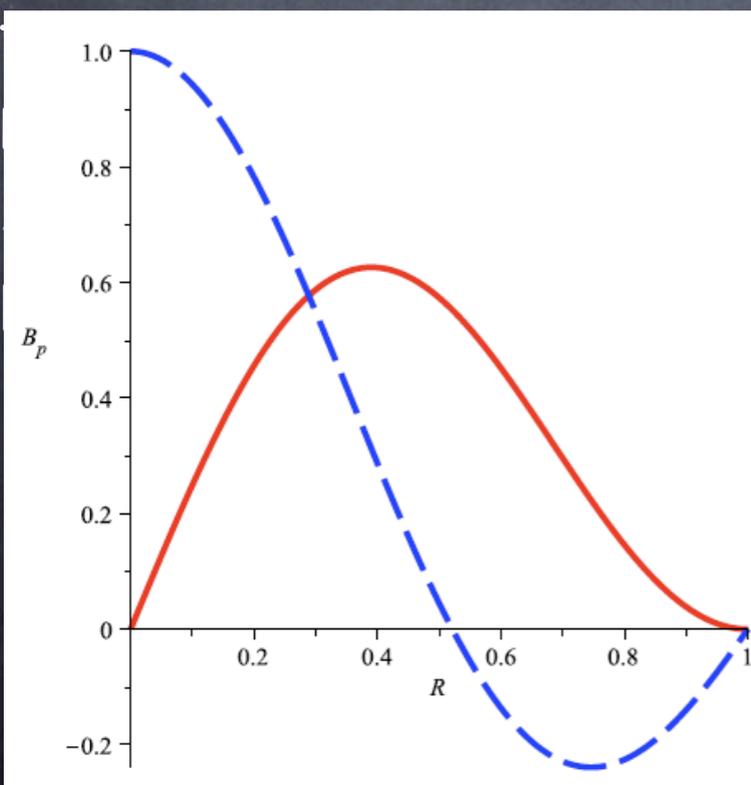
$$\mathbf{B}_{FF} = c_0 \alpha (J_1(\alpha R) \hat{\phi} + J_0(\alpha R) \hat{z})$$



In the G-S case there are two classes of solutions. The choice of the poloidal or toroidal flux is given by the equation  $\frac{R}{2}(B_z^2 + B_\phi^2 + 8\pi p)' + B_\phi^2 = 0$ .

$$B_p = (c_p \alpha_p J_1(\alpha_p R) - \frac{F_p R}{\alpha_p}) \hat{\phi} + (c_p \alpha_p J_0(\alpha_p R) - \frac{2F_p}{\alpha_p^2}) \hat{z}$$

$$B_t = c_t \alpha_t J_1(\alpha_t R) \hat{\phi} + (c_t \alpha_t J_0(\alpha_t R) - \frac{F_t}{\alpha_t}) \hat{z}$$



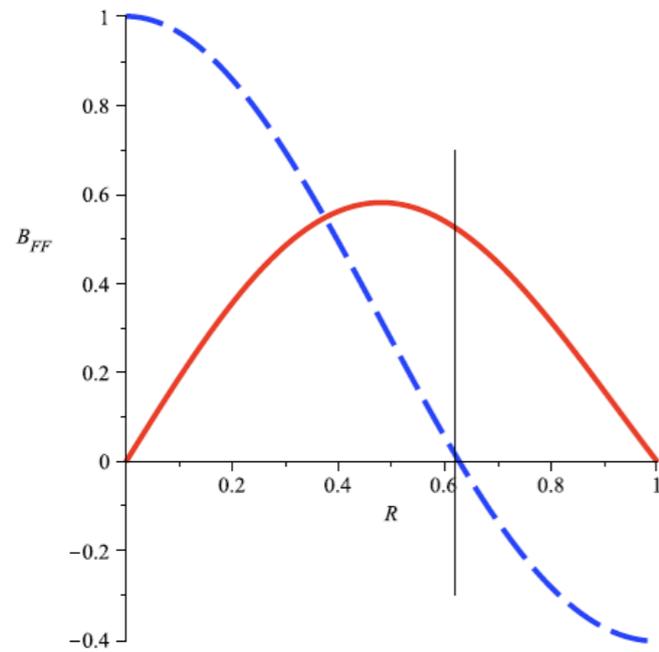
We can construct two basic families of solutions, where both the toroidal and the poloidal field are zero at the boundary of the cylinder.

For the Force-Free case, for a linear relation between  $P$  and  $I$ , there is the Lundquist (1951) solution

$$\nabla \times \mathbf{B} = \alpha \mathbf{B}$$

$$I_{p,t} = \alpha_{p,t} P_{p,t}$$

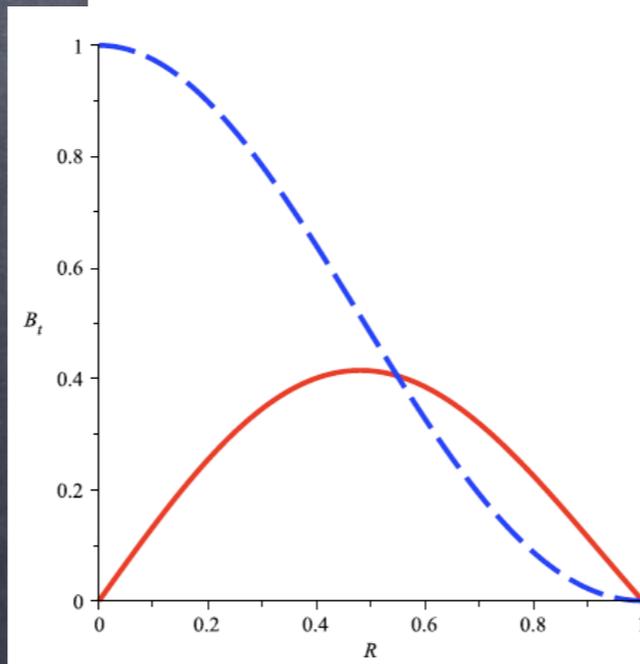
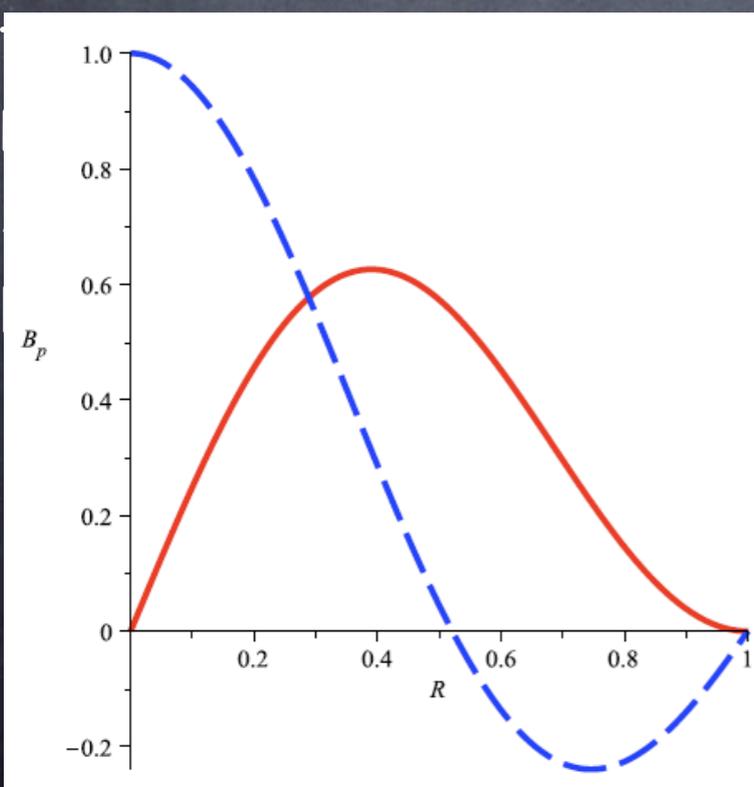
$$\mathbf{B}_{FF} = c_0 \alpha (J_1(\alpha R) \hat{\phi} + J_0(\alpha R) \hat{z})$$



In the G-S case there are two classes of solutions. The choice of the poloidal or toroidal flux is given by the equation  $\frac{R}{2}(B_z^2 + B_\phi^2 + 8\pi p)' + B_\phi^2 = 0$ .

$$B_p = (c_p \alpha_p J_1(\alpha_p R) - \frac{F_p R}{\alpha_p}) \hat{\phi} + (c_p \alpha_p J_0(\alpha_p R) - \frac{2F_p}{\alpha_p^2}) \hat{z}$$

$$B_t = c_t \alpha_t J_1(\alpha_t R) \hat{\phi} + (c_t \alpha_t J_0(\alpha_t R) - \frac{F_t}{\alpha_t}) \hat{z}$$



We can construct two basic families of solutions, where both the toroidal and the poloidal field are zero at the boundary of the cylinder.

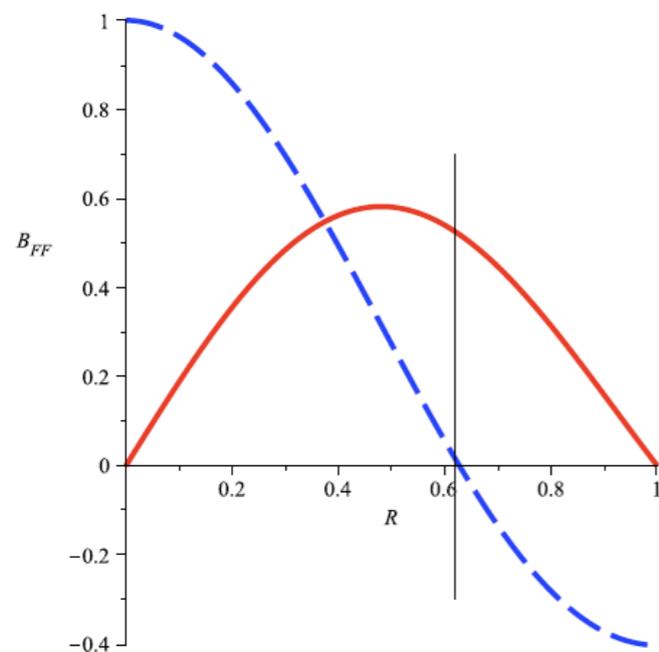
To ensure the absence of current sheets we need a minimum pressure

For the Force-Free case, for a linear relation between  $P$  and  $I$ , there is the Lundquist (1951) solution

$$\nabla \times \mathbf{B} = \alpha \mathbf{B}$$

$$I_{p,t} = \alpha_{p,t} P_{p,t}$$

$$\mathbf{B}_{FF} = c_0 \alpha (J_1(\alpha R) \hat{\phi} + J_0(\alpha R) \hat{z})$$

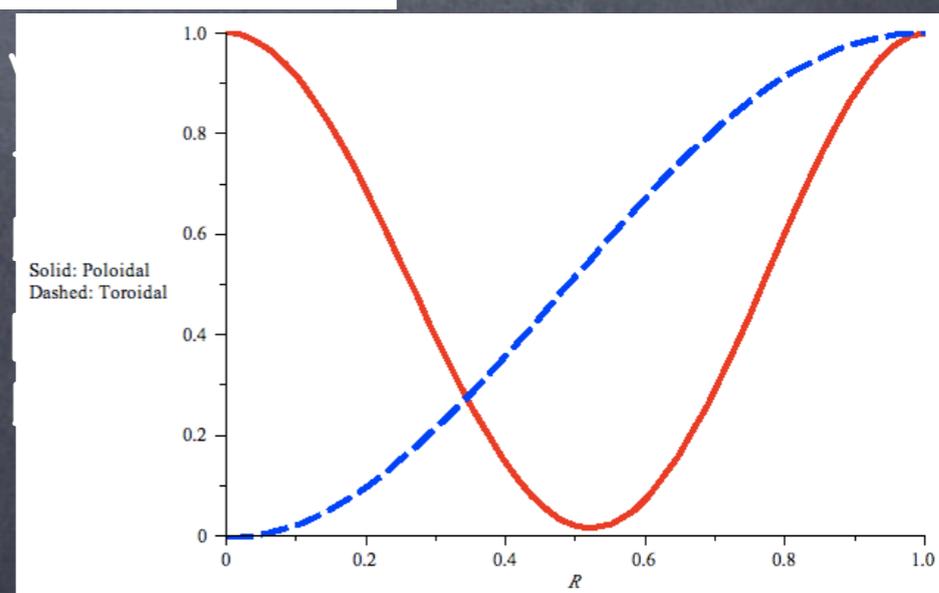
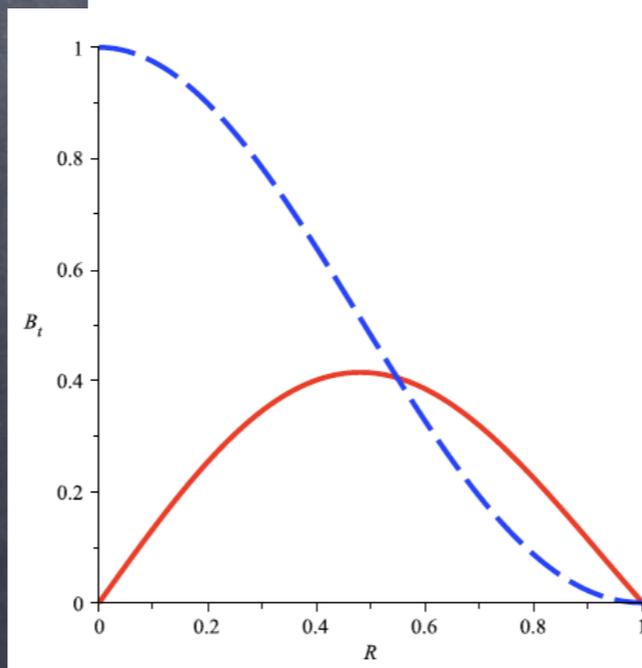
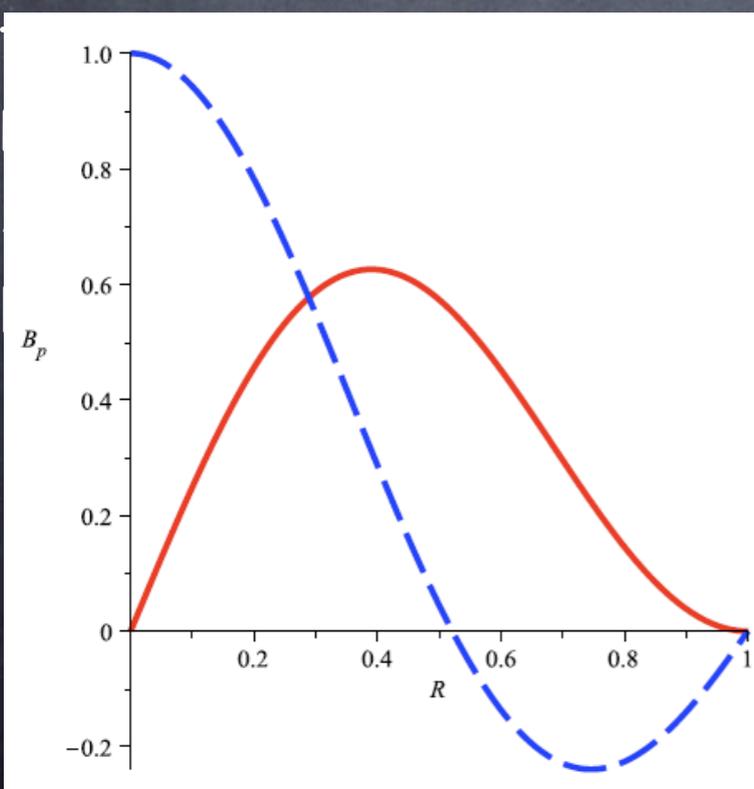


In the G-S case there are two classes of solutions. The choice of the parameter  $\alpha$  determines the location of the poloidal or toroidal maximum.

$$\frac{R}{2} (B_z^2 + B_\phi^2 + 8\pi p)' + B_\phi^2 = 0$$

$$B_p = (c_p \alpha_p J_1(\alpha_p R) - \frac{F_p R}{\alpha_p}) \hat{\phi} + (c_p \alpha_p J_0(\alpha_p R) - \frac{2F_p}{\alpha_p^2}) \hat{z}$$

$$B_t = c_t \alpha_t J_1(\alpha_t R) \hat{\phi} + (c_t \alpha_t J_0(\alpha_t R) - \frac{F_t}{\alpha_t}) \hat{z}$$



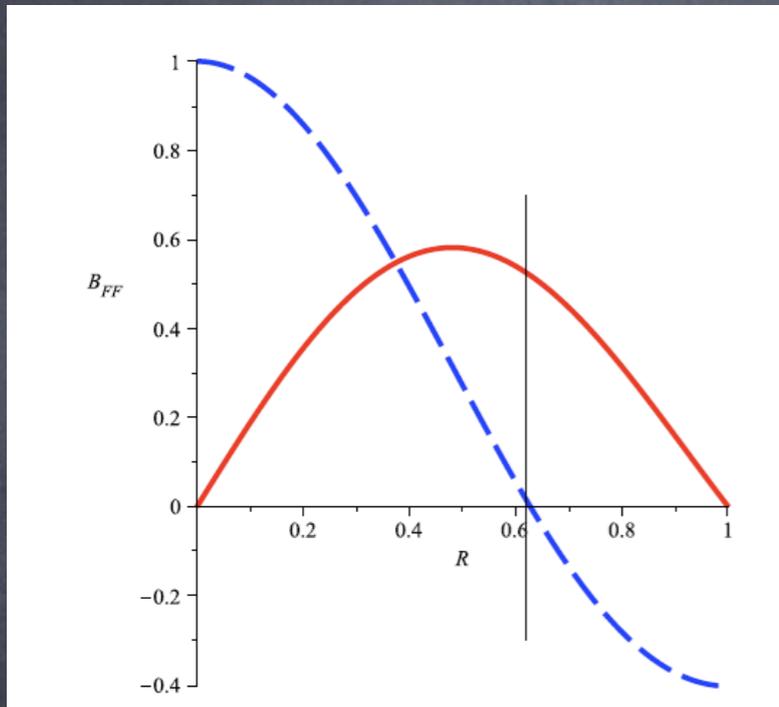
For the G-S case we need a minimum pressure

For the Force-Free case, for a linear relation between  $P$  and  $I$ , there is the Lundquist (1951) solution

$$\nabla \times \mathbf{B} = \alpha \mathbf{B}$$

$$I_{p,t} = \alpha_{p,t} P_{p,t}$$

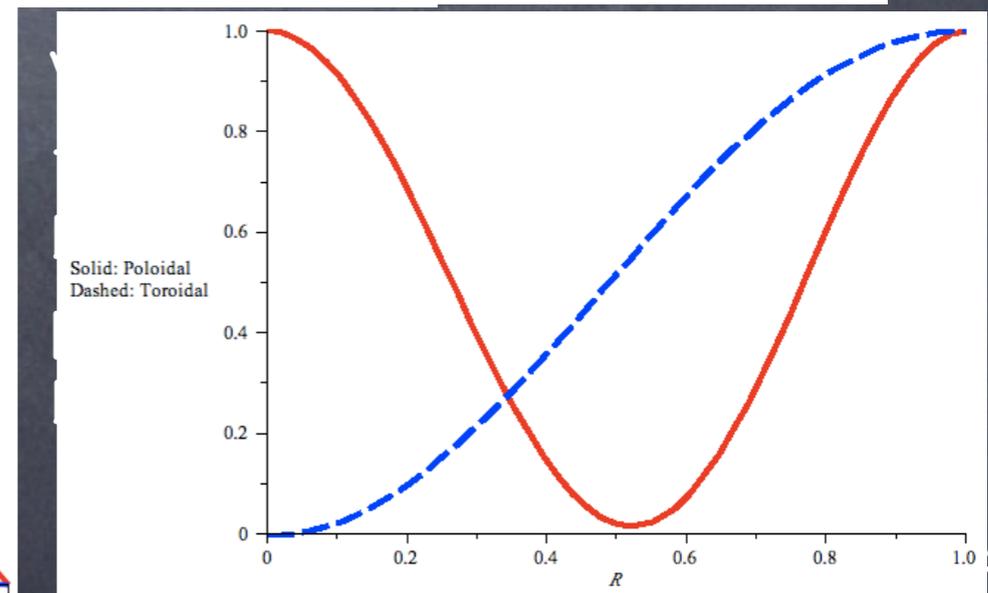
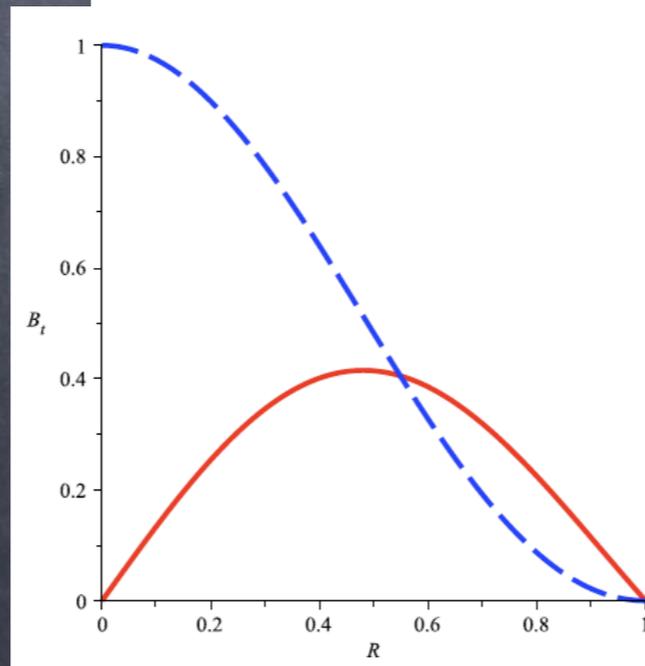
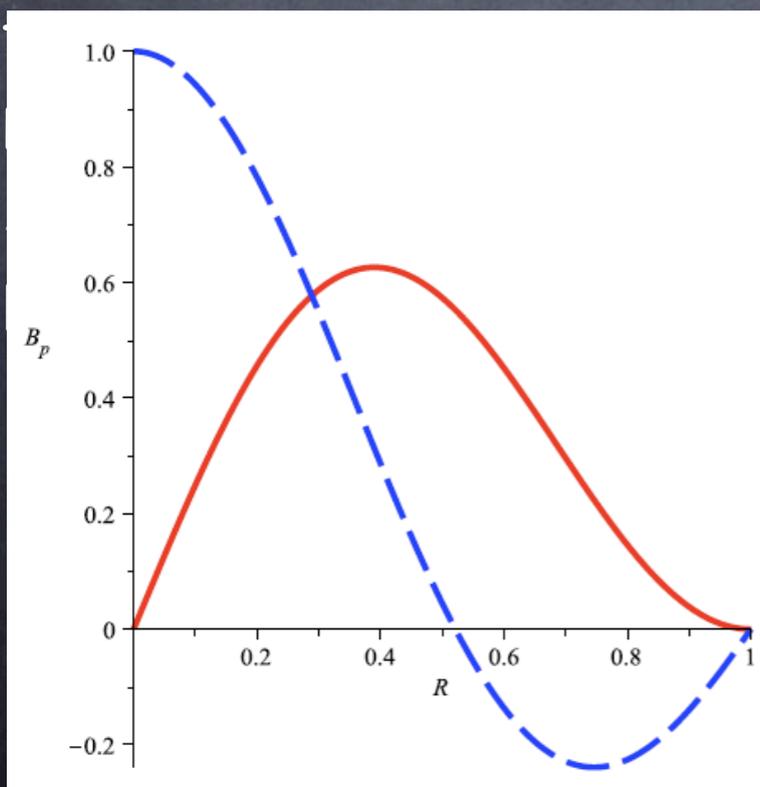
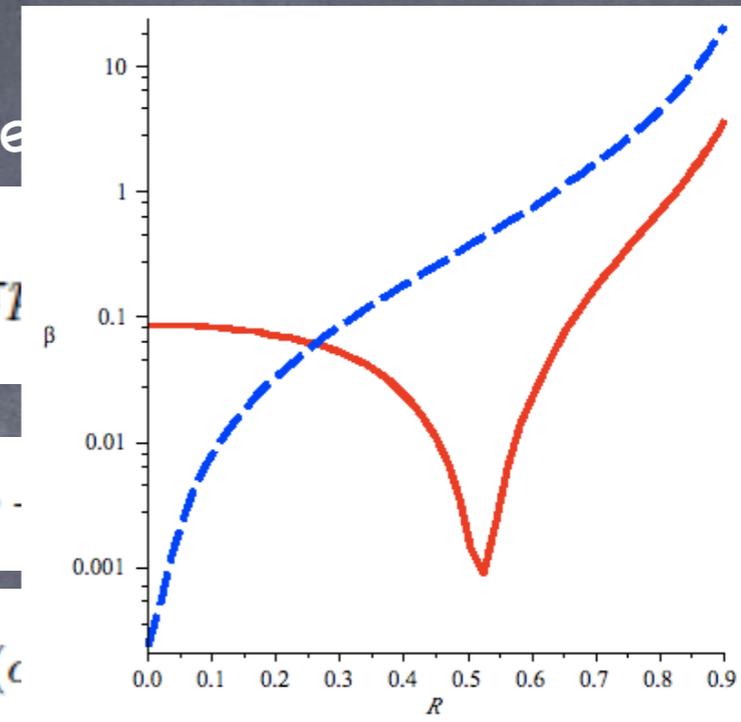
$$\mathbf{B}_{FF} = c_0 \alpha (J_1(\alpha R) \hat{\phi} + J_0(\alpha R) \hat{z})$$



In the G-S case there are solutions of the form  $\frac{R}{2}(B_z^2 + B_\phi^2 + 8\pi p)$  or toroidal flux

$$B_p = (c_p \alpha_p J_1(\alpha_p R) - \frac{F_p R}{\alpha_p}) \hat{\phi}$$

$$B_t = c_t \alpha_t J_1(\alpha_t R) \hat{\phi} + (c_t \alpha_t J_0(\alpha_t R) + \frac{F_t R}{\alpha_t}) \hat{z}$$



... sheets we need a minimum pressure

# Relativistic Case

# Relativistic Case

Motion along the  $z$  axis  
induces electric field

# Relativistic Case

Motion along the z axis  
induces electric field

$$\mathbf{E} = E_R(R) \hat{\mathbf{R}}$$

# Relativistic Case

Motion along the z axis  
induces electric field

$$\mathbf{E} = E_R(R) \hat{\mathbf{R}}$$

$$E_R = v_z B_\phi$$

# Relativistic Case

Motion along the z axis  
induces electric field

$$\mathbf{E} = E_R(R) \hat{\mathbf{R}}$$

$$E_R = v_z B_\phi$$

$$\frac{R}{2} (B_z^2 + B_\phi^2 - E_R^2 + 8\pi p)' + B_\phi^2 - E_R^2 = 0$$

# Relativistic Case

Motion along the z axis  
induces electric field

$$\mathbf{E} = E_R(R) \hat{\mathbf{R}}$$

$$E_R = v_z B_\phi$$

$$\frac{R}{2} (B_z^2 + B_\phi^2 - E_R^2 + 8\pi p)' + B_\phi^2 - E_R^2 = 0$$

$$\frac{R}{2} (B_z^2 + B_\phi^2 + 8\pi p)' + B_\phi^2 = 0$$

# Relativistic Case

Motion along the z axis  
induces electric field

$$\mathbf{E} = E_R(R) \hat{\mathbf{R}}$$

$$E_R = v_z B_\phi$$

$$\frac{R}{2} (B_z^2 + B_\phi^2 - E_R^2 + 8\pi p)' + B_\phi^2 - E_R^2 = 0$$

$$\frac{R}{2} (B_z^2 + B_\phi^2 + 8\pi p)' + B_\phi^2 = 0$$

$$H^2 = B_\phi^2 - E_R^2$$

# Relativistic Case

Motion along the z axis  
induces electric field

$$\mathbf{E} = E_R(R) \hat{\mathbf{R}}$$

$$E_R = v_z B_\phi$$

$$\frac{R}{2} (B_z^2 + B_\phi^2 - E_R^2 + 8\pi p)' + B_\phi^2 - E_R^2 = 0$$

$$H^2 = B_\phi^2 - E_R^2$$

# Relativistic Case

Motion along the z axis  
induces electric field

$$\mathbf{E} = E_R(R) \hat{\mathbf{R}}$$

$$E_R = v_z B_\phi$$

$$\frac{R}{2} (B_z^2 + B_\phi^2 - E_R^2 + 8\pi p)' + B_\phi^2 - E_R^2 = 0$$

$$\frac{R}{2} (B_z^2 + H^2 + 8\pi p)' + H^2 = 0$$

$$H^2 = B_\phi^2 - E_R^2$$

# Relativistic Case

Motion along the z axis  
induces electric field

$$\mathbf{E} = E_R(R) \hat{\mathbf{R}}$$

$$E_R = v_z B_\phi$$

$$\frac{R}{2} (B_z^2 + B_\phi^2 - E_R^2 + 8\pi p)' + B_\phi^2 - E_R^2 = 0$$

$$\frac{R}{2} (B_z^2 + H^2 + 8\pi p)' + H^2 = 0$$

$$H^2 = B_\phi^2 - E_R^2$$

Using the same means as  
in the static case we can  
solve the relativistic

Solution

# Solution

$$E_R = \frac{v_z}{(1 - v_z^2)^{1/2}} \left( c_p \alpha_p J_1(\alpha_p R) - \frac{F_p R}{\alpha_p} \right)$$

$$B_\phi = \frac{1}{(1 - v_z^2)^{1/2}} \left( c_p \alpha_p J_1(\alpha_p R) - \frac{F_p R}{\alpha_p} \right)$$

$$B_z = c_p \alpha_p J_0(\alpha_p R) - \frac{2F_p}{\alpha_p^2},$$

$$p = \frac{1}{4\pi} F_p \left( c_p R J_1(\alpha_p R) - \frac{F_p R^2}{\alpha_p^2} \right) + p_{p,0}$$

# Solution

$$E_R = \frac{v_z}{(1 - v_z^2)^{1/2}} \left( c_p \alpha_p J_1(\alpha_p R) - \frac{F_p R}{\alpha_p} \right)$$

$$B_\phi = \frac{1}{(1 - v_z^2)^{1/2}} \left( c_p \alpha_p J_1(\alpha_p R) - \frac{F_p R}{\alpha_p} \right)$$

$$B_z = c_p \alpha_p J_0(\alpha_p R) - \frac{2F_p}{\alpha_p^2},$$

$$p = \frac{1}{4\pi} F_p \left( c_p R J_1(\alpha_p R) - \frac{F_p R^2}{\alpha_p^2} \right) + p_{p,0}$$

$$E_R = \frac{v_z}{(1 - v_z^2)^{1/2}} c_t \alpha_t J_1(\alpha_t R),$$

$$B_\phi = \frac{1}{(1 - v_z^2)^{1/2}} c_t \alpha_t J_1(\alpha_t R),$$

$$B_z = \alpha_t \left( c_t J_0(\alpha_t R) - \frac{F_t}{\alpha_t^2} \right),$$

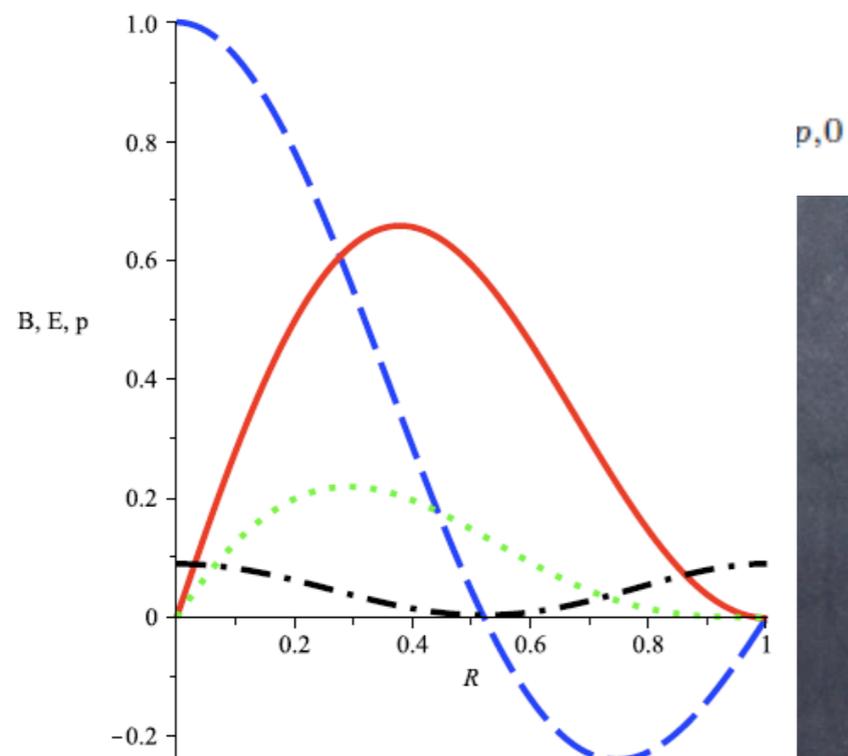
$$p = \frac{1}{4\pi} F_t \left( c_t J_0(\alpha_t R) - \frac{F_t}{\alpha_t^2} \right) + p_{t,0}$$

# Solution

$$E_R = \frac{v_z}{(1 - v_z^2)^{1/2}} \left( c_p \alpha_p J_1(\alpha_p R) - \frac{F_p R}{\alpha_p} \right)$$

$$B_\phi = \frac{1}{(1 - v_z^2)^{1/2}} \left( c_p \alpha_p J_1(\alpha_p R) - \frac{F_p R}{\alpha_p} \right)$$

$$B_z = c_p \alpha_p J_0(\alpha_p R) - \frac{2F_p}{\alpha_p}$$



$$E_R = \frac{v_z}{(1 - v_z^2)^{1/2}} c_t \alpha_t J_1(\alpha_t R),$$

$$B_\phi = \frac{1}{(1 - v_z^2)^{1/2}} c_t \alpha_t J_1(\alpha_t R),$$

$$B_z = \alpha_t \left( c_t J_0(\alpha_t R) - \frac{F_t}{\alpha_t^2} \right),$$

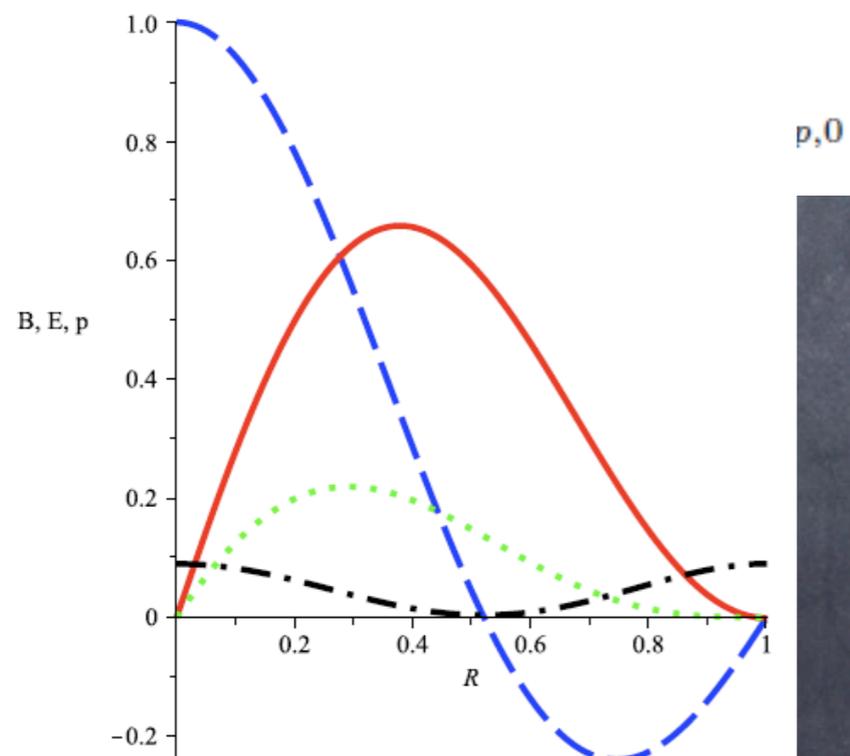
$$p = \frac{1}{4\pi} F_t \left( c_t J_0(\alpha_t R) - \frac{F_t}{\alpha_t^2} \right) + p_{t,0}$$

# Solution

$$E_R = \frac{v_z}{(1 - v_z^2)^{1/2}} \left( c_p \alpha_p J_1(\alpha_p R) - \frac{F_p R}{\alpha_p} \right)$$

$$B_\phi = \frac{1}{(1 - v_z^2)^{1/2}} \left( c_p \alpha_p J_1(\alpha_p R) - \frac{F_p R}{\alpha_p} \right)$$

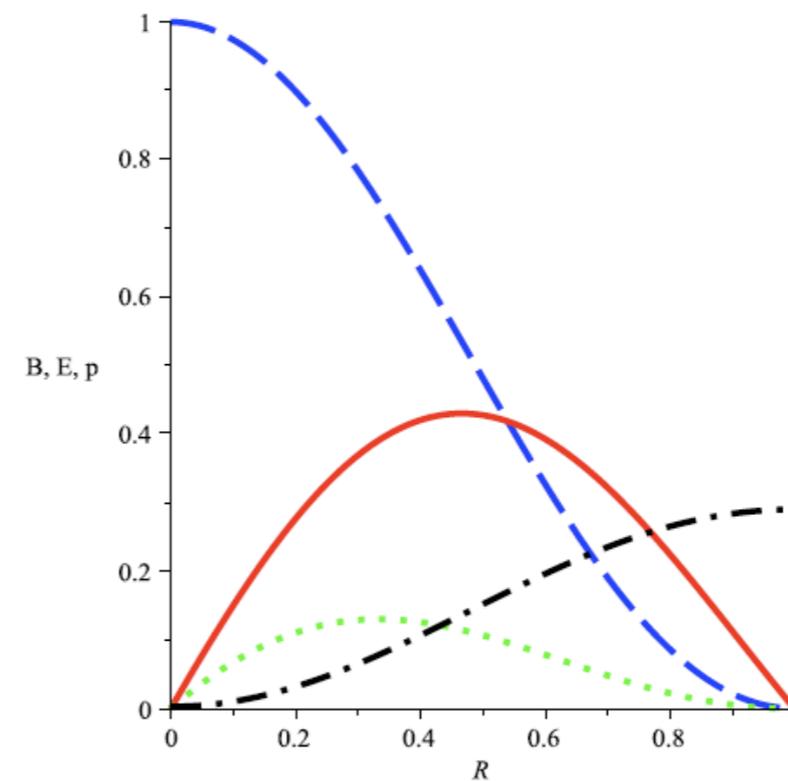
$$B_z = c_p \alpha_p J_0(\alpha_p R) - \frac{2F_p}{\alpha},$$



$$E_R = \frac{v_z}{(1 - v_z^2)^{1/2}} c_t \alpha_t J_1(\alpha_t R),$$

$$B_\phi = \frac{1}{(1 - v_z^2)^{1/2}} c_t \alpha_t J_1(\alpha_t R),$$

$$B_z = \alpha_t \left( c_t J_0(\alpha_t R) - \frac{F_t}{-2} \right),$$



# Velocity

# Velocity

In the solution we have assumed an axial velocity,  
parallel to the  $z$  direction

# Velocity

In the solution we have assumed an axial velocity, parallel to the z direction

$$\mathbf{v} = v_z \hat{\mathbf{z}}$$

# Velocity

In the solution we have assumed an axial velocity, parallel to the z direction

$$\mathbf{v} = v_z \hat{\mathbf{z}}$$

The  $\mathbf{E} \times \mathbf{B}$  velocity from the induced electric field gives a toroidal component

# Velocity

In the solution we have assumed an axial velocity, parallel to the z direction

$$\mathbf{v} = v_z \hat{\mathbf{z}}$$

The  $\mathbf{E} \times \mathbf{B}$  velocity from the induced electric field gives a toroidal component

$$\mathbf{V}_F = \frac{\mathbf{E} \times \mathbf{B}}{B^2} = \frac{(-\mathbf{v} \times \mathbf{B}) \times \mathbf{B}}{B^2} = \mathbf{v} - \frac{\mathbf{v} \cdot \mathbf{B}}{B^2} \mathbf{B}$$

# Velocity

In the solution we have assumed an axial velocity, parallel to the z direction

$$\mathbf{v} = v_z \hat{\mathbf{z}}$$

The  $\mathbf{E} \times \mathbf{B}$  velocity from the induced electric field gives a toroidal component

$$\begin{aligned} \mathbf{V}_F &= \frac{\mathbf{E} \times \mathbf{B}}{B^2} = \frac{(-\mathbf{v} \times \mathbf{B}) \times \mathbf{B}}{B^2} = \mathbf{v} - \frac{\mathbf{v} \cdot \mathbf{B}}{B^2} \mathbf{B} \\ &= -\frac{v_z B_\phi B_z}{B^2} \hat{\phi} + \frac{v_z B_\phi^2}{B^2} \hat{\mathbf{z}}. \end{aligned}$$

# Velocity

In the solution we have assumed an axial velocity, parallel to the z direction

$$\mathbf{v} = v_z \hat{\mathbf{z}}$$

The  $\mathbf{E} \times \mathbf{B}$  velocity from the induced electric field gives a toroidal component

$$\mathbf{V}_F = \frac{\mathbf{E} \times \mathbf{B}}{B^2} = \frac{(-\mathbf{v} \times \mathbf{B}) \times \mathbf{B}}{B^2} = \mathbf{v} - \frac{\mathbf{v} \cdot \mathbf{B}}{B^2} \mathbf{B}$$

$$= -\frac{v_z B_\phi B_z}{B^2} \hat{\phi} + \frac{v_z B_\phi^2}{B^2} \hat{\mathbf{z}}.$$

The difference is from the projection of the velocity along the magnetic field

# Velocity

In the solution we have assumed an axial velocity, parallel to the z direction

$$\mathbf{v} = v_z \hat{\mathbf{z}}$$

The  $\mathbf{E} \times \mathbf{B}$  velocity from the induced electric field gives a toroidal component

$$\mathbf{V}_F = \frac{\mathbf{E} \times \mathbf{B}}{B^2} = \frac{(-\mathbf{v} \times \mathbf{B}) \times \mathbf{B}}{B^2} = \mathbf{v} - \frac{\mathbf{v} \cdot \mathbf{B}}{B^2} \mathbf{B}$$

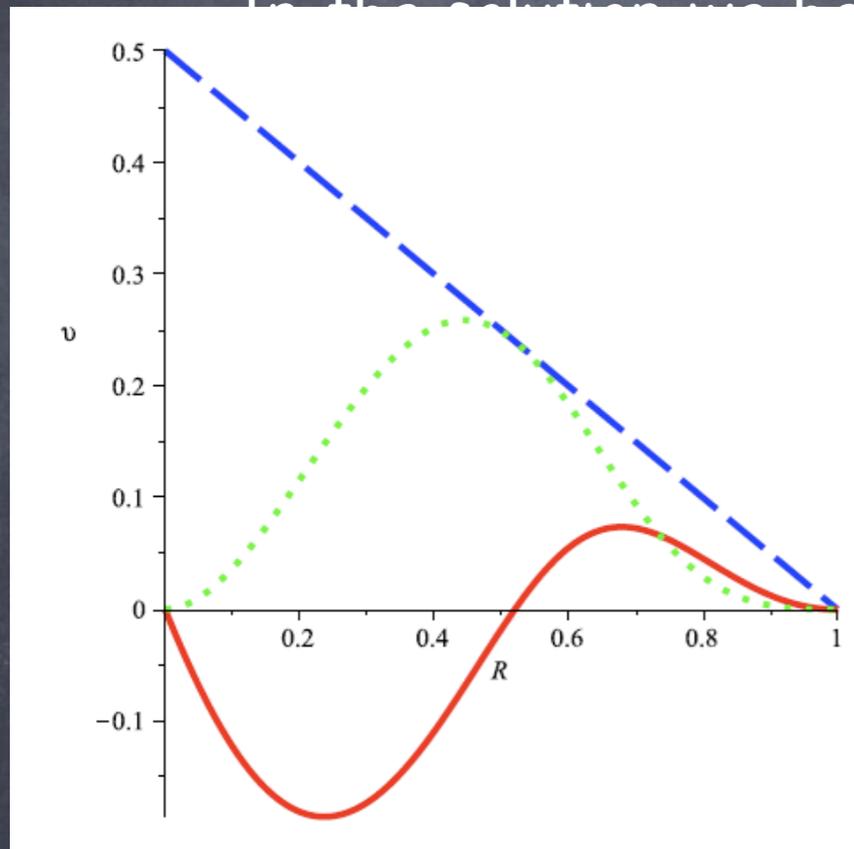
$$= -\frac{v_z B_\phi B_z}{B^2} \hat{\phi} + \frac{v_z B_\phi^2}{B^2} \hat{\mathbf{z}}.$$

The difference is from the projection of the velocity along the magnetic field

The  $\mathbf{V}_F$  velocity depends on the details of the magnetic field structure

# Velocity

In the solution we have assumed an axial velocity,  $\mathbf{v} = v_z \hat{\mathbf{z}}$



$$\mathbf{v} = v_z \hat{\mathbf{z}}$$

from the induced electric field component

$$\mathbf{v} \times \mathbf{B} = \mathbf{v} - \frac{\mathbf{v} \cdot \mathbf{B}}{B^2} \mathbf{B}$$

$\mathbf{v} = -\frac{\tilde{\tau}}{B^2} \nabla \phi + \frac{\tilde{\tau}}{B^2} \hat{\mathbf{z}}$ . The difference is from the projection of the velocity along the magnetic field

The  $\mathbf{V}_F$  velocity depends on the details of the magnetic field structure

# Velocity

In the solution we have assumed

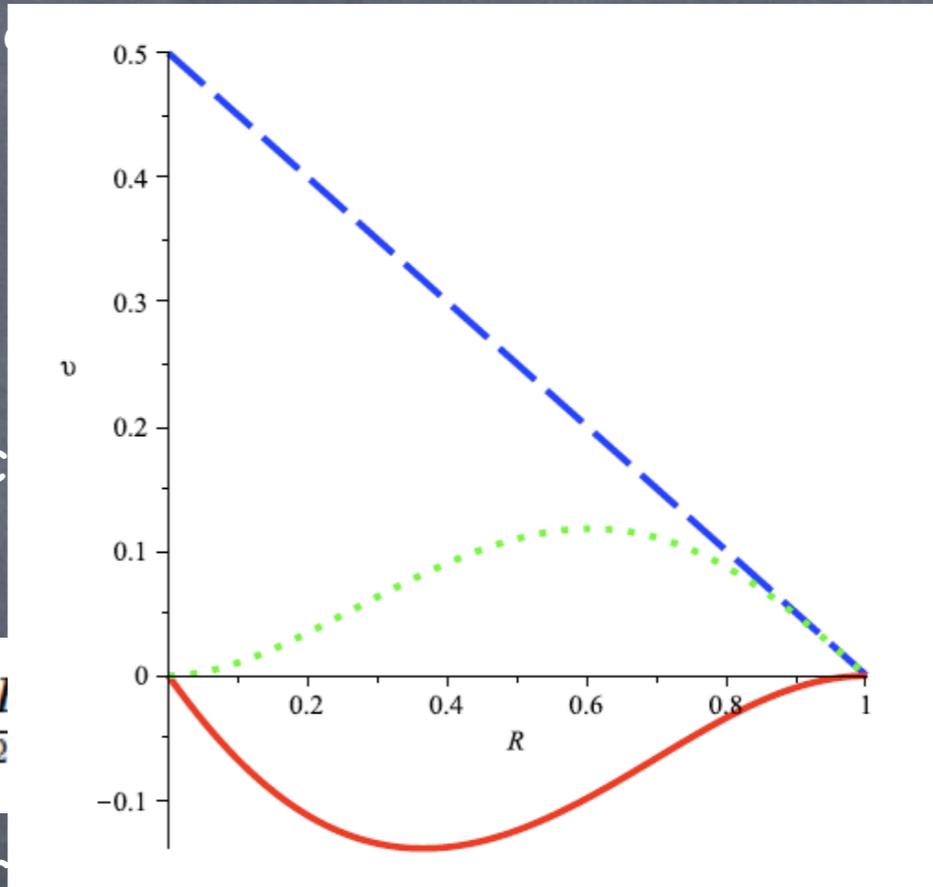
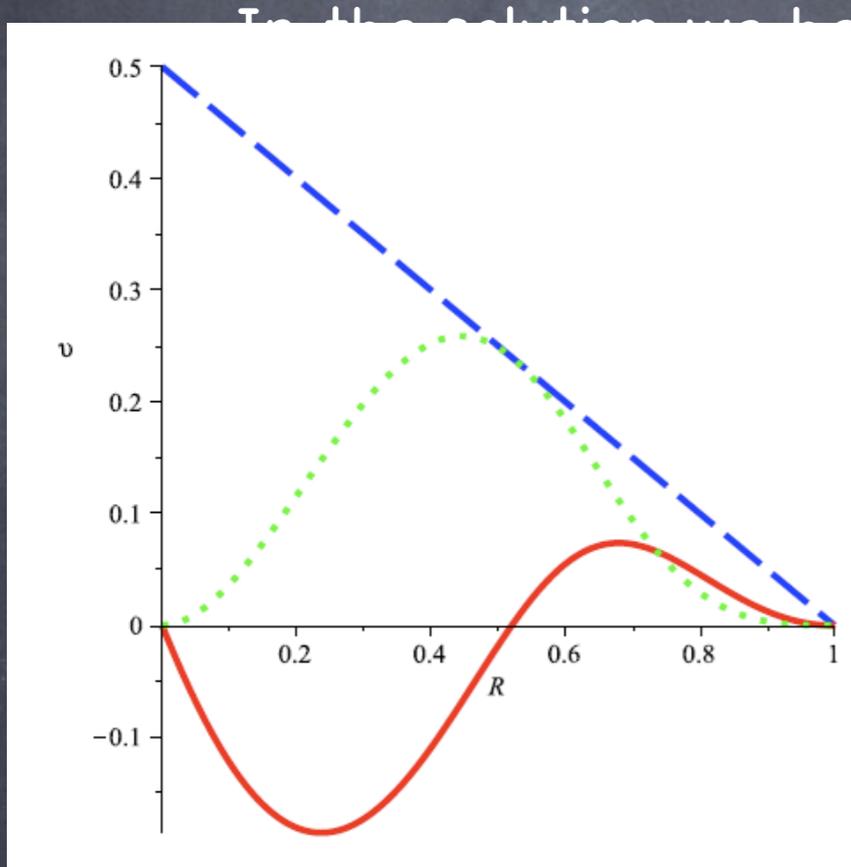
$$\mathbf{v} = v_z \hat{\mathbf{z}}$$

from the induction equation

$$\nabla \times \mathbf{B} = \mathbf{v} \times \hat{\mathbf{z}} - \frac{\mathbf{v} \cdot \nabla \mathbf{B}}{B^2}$$

$$\mathbf{v} = -\frac{\nabla \phi}{B^2} + \frac{\nabla B^2}{B^2} \hat{\mathbf{z}}$$

The difference between the projection of the velocity along the magnetic field



The  $V_F$  velocity depends on the details of the magnetic field structure

# Simulation

# Simulation

An important issue in simulations is the confinement of the jet (Clarke et al. 1986, Lind et al 1989, Stone & Hardee 2000, Mignone et al. 2010)

# Simulation

An important issue in simulations is the confinement of the jet (Clarke et al. 1986, Lind et al 1989, Stone & Hardee 2000, Mignone et al. 2010)

Current sheets are hard to treat numerically, so for the initial state one may choose either a homogeneous background field and inject the helical field or a sinusoidal field in the domain etc

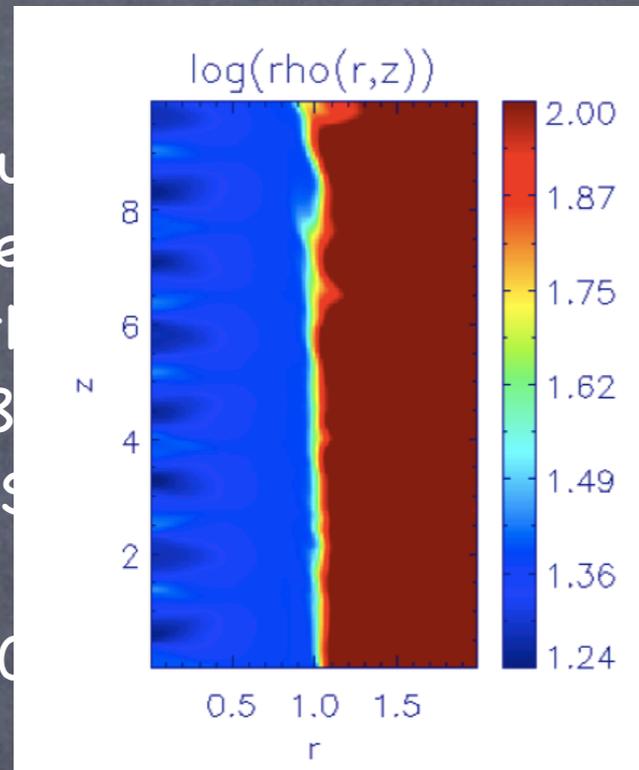
# Simulation

An important issue in simulations is the confinement of the jet (Clarke et al. 1986, Lind et al 1989, Stone & Hardee 2000, Mignone et al. 2010)

Current sheets are hard to treat numerically, so for the initial state one may choose either a homogeneous background field and inject the helical field or a sinusoidal field in the domain etc

In this study we assume a given ambient pressure and we inject the solution we have found in the PLUTO code (Mignone et al. 2007)

# Simulation



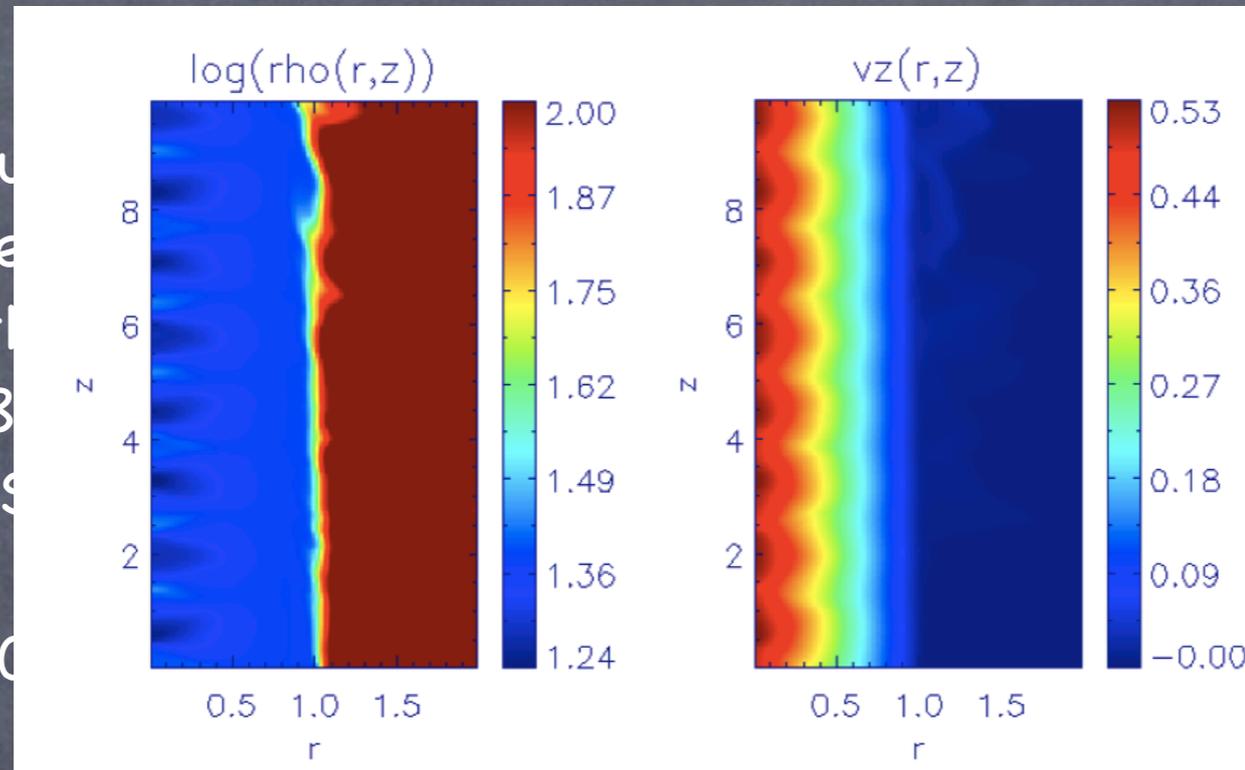
An important issue in  
simulations is the  
confinement of the  
(Clarke et al. 1988,  
Lind et al 1989, S  
& Hardee 2000,  
Mignone et al. 2007)

Current sheets are hard to treat  
numerically, so for the initial  
state one may choose either a  
homogeneous background field  
and inject the helical field or a  
sinusoidal field in the domain etc

In this study we assume  
a given ambient pressure  
and we inject the  
solution we have found  
in the PLUTO code  
(Mignone et al. 2007)

# Simulation

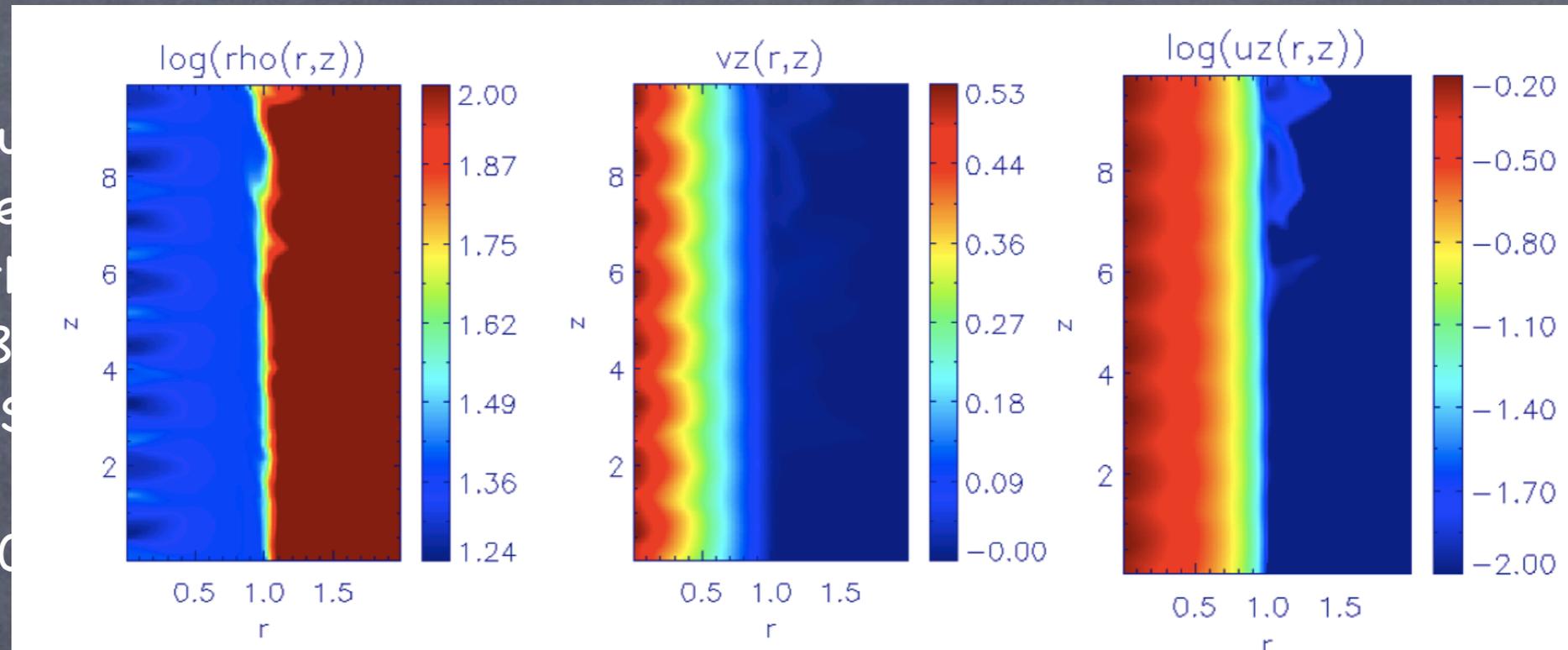
An important issue in magnetohydrodynamic (MHD) simulations is the confinement of the current sheet. (Clarke et al. 1988, Lind et al 1989, S. & Hardee 2000, Mignone et al. 2007)



Current sheets are hard to treat numerically, so for the initial state one may choose either a homogeneous background field and inject the helical field or a sinusoidal field in the domain etc

In this study we assume a given ambient pressure and we inject the solution we have found in the PLUTO code (Mignone et al. 2007)

# Simulation

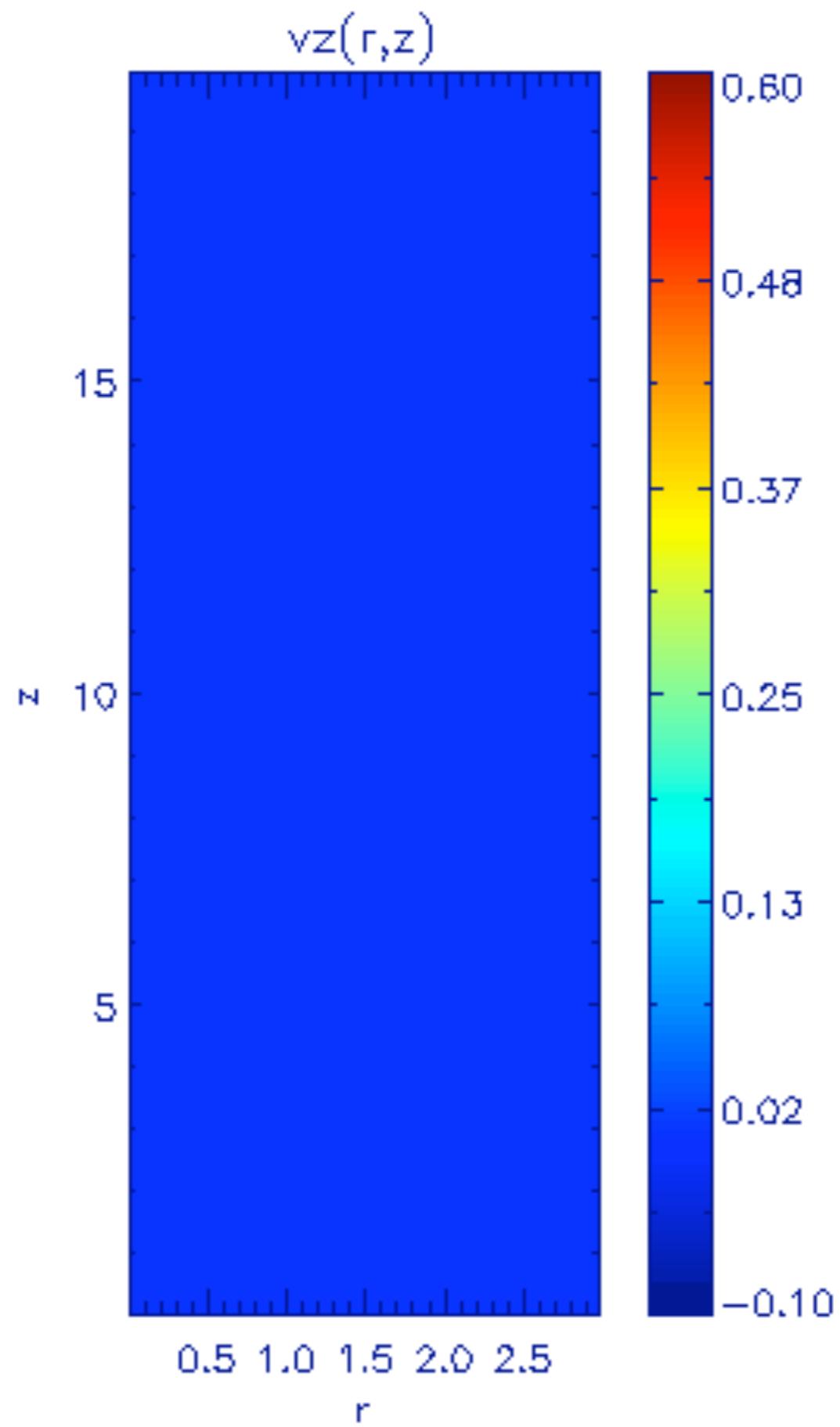


An important issue in these simulations is the confinement of the current sheet (Clarke et al. 1988, Lind et al 1989, Sulem & Hardee 2000, Mignone et al. 2007)

Current sheets are hard to treat numerically, so for the initial state one may choose either a homogeneous background field and inject the helical field or a sinusoidal field in the domain etc

In this study we assume a given ambient pressure and we inject the solution we have found in the PLUTO code (Mignone et al. 2007)





# Stability

# Stability

- In the 2-D simulations the overall behaviour is stable

# Stability

- In the 2-D simulations the overall behaviour is stable
- The kink-instability however cannot be investigated through 2-D simulations

# Stability

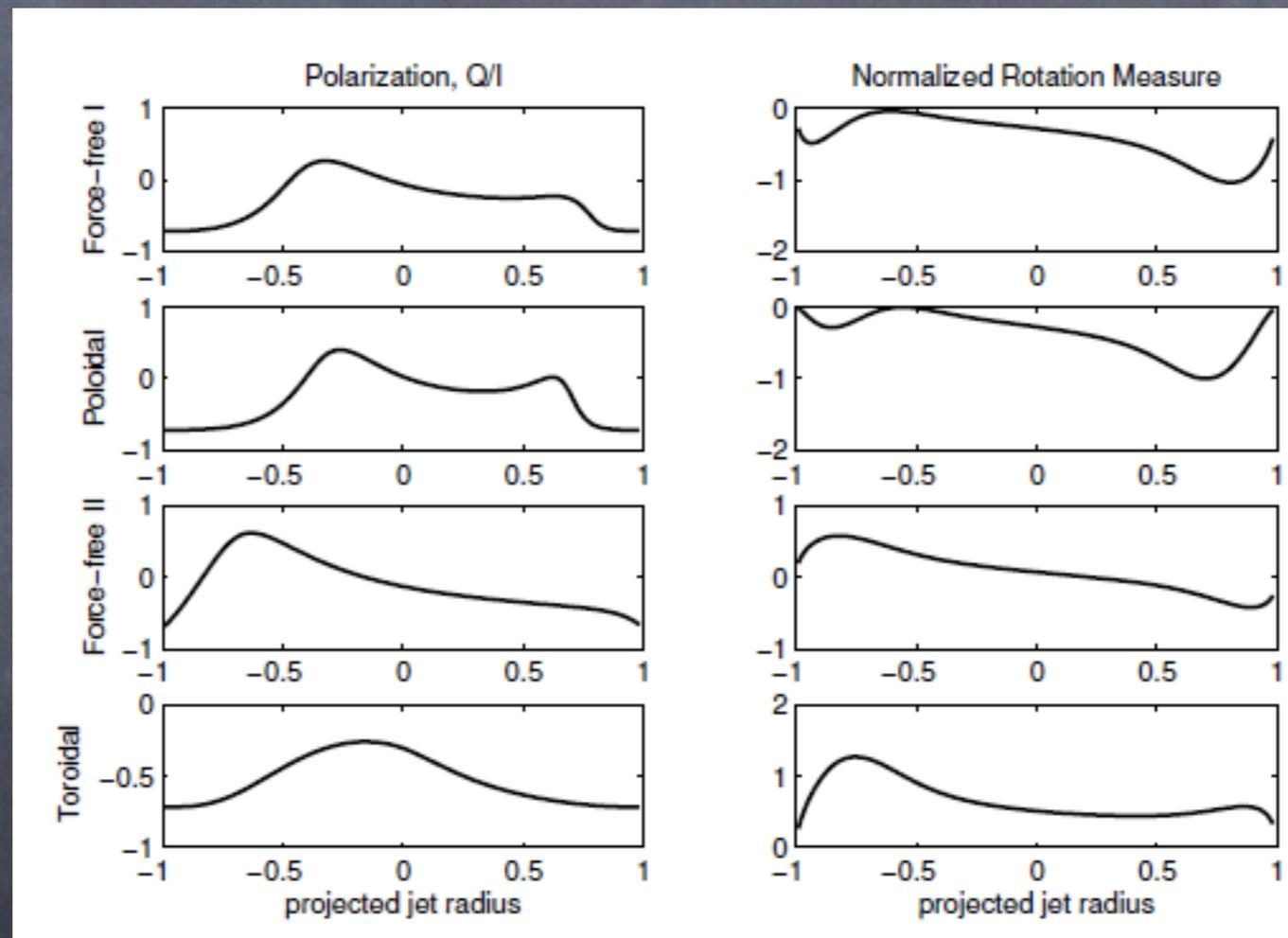
- In the 2-D simulations the overall behaviour is stable
- The kink-instability however cannot be investigated through 2-D simulations
- From the Kruskal-Shafranov and the Suydam criteria we expect some unstable regions in the "poloidal" equilibrium

# Stability

- In the 2-D simulations the overall behaviour is stable
- The kink-instability however cannot be investigated through 2-D simulations
- From the Kruskal-Shafranov and the Suydam criteria we expect some unstable regions in the "poloidal" equilibrium
- The velocity shear stabilizes and suppresses some instabilities

# Polarization

# Polarization



# Conclusions

# Conclusions

- We have explored a class of solutions of the G-S equation in static and relativistic context

# Conclusions

- We have explored a class of solutions of the G-S equation in static and relativistic context
- The solutions without current sheets are particularly useful for simulations as initial conditions or test configurations

# Conclusions

- We have explored a class of solutions of the G-S equation in static and relativistic context
- The solutions without current sheets are particularly useful for simulations as initial conditions or test configurations
- They answer the question of the pressure lying between the pure hydro models and the magnetic models

# Conclusions

- We have explored a class of solutions of the G-S equation in static and relativistic context
- The solutions without current sheets are particularly useful for simulations as initial conditions or test configurations
- They answer the question of the pressure lying between the pure hydro models and the magnetic models
- In the observational side they do not have significant differences from the Force-Free structures used

Thanks